

**NUMERICAL INVESTIGATION OF  
FLOW PAST A SPHERE**

*BY*

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**M.TECH/SSSE/2000/2001/583**

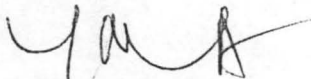
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MINNA**

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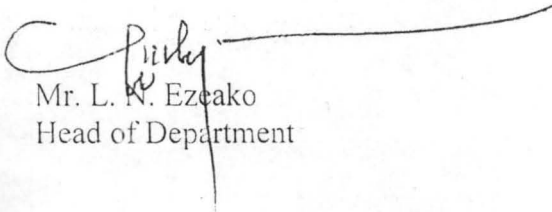
## CERTIFICATION

This thesis titled "NUMERICAL INVESTIGATION OF FLOW PAST A SPHERE" by Abah, Sunday Ojima, meets the regulations governing the award of the degree of Masters of Technology in Mathematics. Federal University of Minna and is approved for its contribution to knowledge and literary presentation.



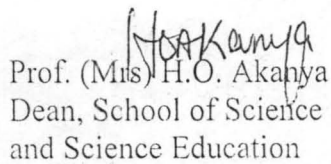
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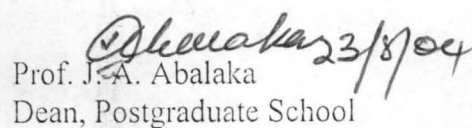
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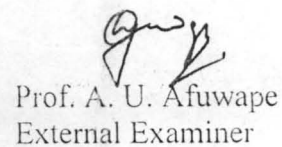
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# DEDICATION

This research work is dedicated to the Almighty God; and my family.

# ACKNOWLEDGEMENT

I would like to express my profound gratitude to all those who contributed to the successful completion of my academic goal of this nature, especially my parents Mr. And Mrs. Usman Abah and family members.

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# ABSTRACT

In this research work, Numerical Investigation of Flow Past a Sphere we consider the flow of fluid past a sphere at low Reynolds number. Assuming the flow is steady and asymmetrical within the vicinity of the sphere. We neglect the Inertia terms and assume the absences of extraneous forces.

The method of regular perturbation analysis is being used in linearizing the governing equation; the resulting equation was solved analytically. The graphs of the variation of the flow pattern were plotted for specific values of the ratio of the distance from the sphere to the radius of the sphere.

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## CHAPTER ONE

### 1.0 INTRODUCTION

In this research work we consider the flow of an inviscid fluid past a sphere at low Reynolds number. We will assume that flow is steady and axis symmetrical and flow is in the vicinity of the sphere is not valid at large distances from the sphere.

Under this assumption the equation is given by

$$\nabla^2 u - \nabla p = R(v \cdot \nabla)v \quad \nabla v = 0 \dots \dots \dots 1.1$$

Where  $v$  is the pressure,  $R = \frac{ua}{\nu}$  is the Reynolds number.  $\rho$  is the density and  $\nu$  is the kinematic viscosity.

This problem was first solved by Stokes (1851) and Kaplun (1957) using a method of matched asymptotic expansion.

In this research work we neglect inertia terms and assume the absence of extraneous forces so that we have the problem in the form

$$\mu \nabla^2 u = \frac{\partial p}{\partial x} \dots \dots \dots 1.2$$

which is solvable using the method of regular perturbation analysis.

We now proceed to solve the order  $\varepsilon^0$  problem using the method of separation of variable



which results into a Legendre polynomial which we solved using method of series solution.

### 1.1 Definition of Terms

- (i) Fluid: A fluid is a substance which deforms or yields continuously when shear stress is applied to it, no matter how small it is.
- (ii) Incompressible fluid: A fluid is said to be incompressible if the density is invariant with time and space.

$$\frac{d\rho}{dt} = \nabla \rho = 0 \quad \text{Where } \rho \text{ is density}$$

N.B Density ( $\rho$ ) is the mass per unit volume.

- (iii) Compressible fluid: A fluid is compressible if the density depends continuously on the time and space variable.
- (iv) Specific volume is the volume per unit weight
- (v) Viscosity: Viscosity is the property of a fluid by which it offers resistance to shear acting on it. According to Newton's law of Viscosity, the shear  $F$  acting between two layers of fluid is proportional to differences in their velocities and inversely proportional to the distance between them.

$$\text{i.e.} \quad F = \mu A \frac{\Delta u}{\Delta y}$$

$$\Gamma = \frac{F}{A} = \mu \frac{\Delta u}{\Delta y} \quad \text{Which is the shear stress.}$$

Where  $\mu$  is the constant of proportionality

$$\frac{du}{dy} = \text{rate of angular deformation}$$

Fluid are classified according to the relation between shear stress  $\Gamma$  and rate of angular deformation.

(a) Newtonian fluids: are fluid which obeys Newton's law of Viscosity

$$\text{i.e. } \Gamma = \mu \frac{du}{dy} \quad \text{e.g. water and kerosene etc}$$

(b) Non – Newtonian fluids: They do not obey Newton's law of Viscosity

$$\text{i.e. } \Gamma = \mu \frac{(du)^n}{dy}$$

e.g. blood, mud flow, suspensions and polymer solutions.

) Ideal fluids: These are fluids that have no Viscosity, Surface tension and are incompressible     i.e.      $\Gamma = 0$

(d) Idea Plastics or Bingham Plastics: These are fluids where

$$\Gamma = \text{constant} + \mu \frac{du}{dy}$$

(e) Thyxotropic fluids: are fluid where

$$\Gamma = \text{constant} + \mu \frac{(du)^n}{dy}$$

Fluid Mechanics: Fluids mechanics is the branch of engineering science which deals with the behavior of fluids under the conditions of rest and motion.

### 1.2. Kinematics of fluid flow

Kinematics of fluid flows deals with fluid motion in terms of displacements, velocities, acceleration, rotation of fluid without regard to the force or energy responsible for the motion.

If F is a flow or fluid property such as velocity, pressure, mass, density or temperature the following types of flow can be defined:

1 Steady flow:  $\frac{\partial f}{\partial t} = 0$  at a point or section

2. Unsteady flow:  $\frac{\partial f}{\partial t} \neq 0$  at a point or section

3. Uniform flow:  $\frac{\partial f}{\partial s}_{t=t_0} = 0$

4. Non-Uniform flow:  $\frac{\partial f}{\partial s}_{t=t_0} \neq 0$

5. One dimensional flow  $f = f(x,t)$  or  $f(s,t)$

6. Two dimensional flow:  $f = f(x,y,t)$

7. Three dimensional flow:  $f = f(x,y,z,t)$

### 1.2.2 Streamlines Pathline and streaklines

An imaginary line in the flow field such that at every point along it the velocity vector is tangential to it is known as a streamline.

Equation of streamline is

$$\frac{u}{dx} = \frac{v}{dy} = \frac{w}{dz}$$

path line is the path followed by a fluid particle during its travel.

A stream line in the path followed by all the fluid particles passing through a given point in space. A stream tube consist of a group of streamlines.

### 1.2.3 Continuity Equation

The application of the principle conservation of mass to an elementary volume gives continuity equation in any co-ordinate system.

For compressible fluids,

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho_u}{\partial x} + \frac{\partial \rho_v}{\partial y} + \frac{\partial \rho_w}{\partial z} = 0$$

in vector form,  $\frac{\partial \rho}{\partial t} + \nabla(\rho \mathbf{v}) = 0$

for incompressible (homogenous or non homogenous fluids)

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

### 2.4 Acceleration

Acceleration is the rate of change of velocity with time and it is a vector quantity. Convective acceleration is due to non – uniformity of flow where as local acceleration due to unsteadiness of flow. Tangential acceleration.

$$a_s = v_s \frac{\partial v_s}{\partial s}$$

It is along the streamline and it is due to change in magnitude of velocity. Local tangential acceleration is given by

$$\frac{\partial v_s}{\partial t}$$

Total tangential acceleration

$$\frac{\partial v_s}{\partial t} = \frac{\partial v_s}{\partial t} + v_s \frac{\partial v_s}{\partial s}$$

Convective normal acceleration due to change in direction of flow along a streamline is equal to

$$\frac{v_s^2}{R}$$

Where R is the radius of curvature of streamline.

$$\text{Local normal acceleration} = \frac{\partial v_n}{\partial t}$$

Where  $v_n$  normal component of velocity generate due to change in direction.

$$\frac{\partial v_n}{\partial t} = \frac{\partial v_n}{\partial t} + \frac{v_s^2}{R}$$

### 1.2.5 Rotation and circulation

Rotation  $\omega$  about any axis is defined as the average of angular velocities of two elements

The rotation velocity is given by

$$\begin{aligned}\omega &= \omega_x i + \omega_y j + \omega_z k \\ &= \frac{1}{2} \nabla \times \mathbf{v}\end{aligned}$$

Circulation  $\Gamma$  around a close curve  $C$  is defined as the line integral of  $\mathbf{v} \cdot d\mathbf{s}$  along the curve  $C$ , taken positive in anticlockwise direction.

$$\begin{aligned}\Gamma &= \int_C \mathbf{v} \cdot d\mathbf{s} \\ &= \int_C (u dx + v dy + w dz)\end{aligned}$$

the quantity  $2\omega$  is known as Vorticity, which is also a vector quantity. If at every point in the flow  $\omega_x = \omega_y = \omega_z$  is equal to zero, flow is called irrotational otherwise it is rotational flow.

### 1.6 Velocity Potential and Stream Function.

Velocity Potential Function  $\phi$  is a scalar function of any of  $x, y, z$  and  $t$  such that its negative derivative with respect to any of  $x, y, z$  gives the velocity component in that direction.

Thus:

$$\Phi = \phi(x, y, z, t) \text{ and}$$

$$-\frac{\partial \phi}{\partial x} = u$$

$$-\frac{\partial \phi}{\partial y} = v$$

$$-\frac{\partial \phi}{\partial z} = w.$$

for incompressible fluid,  $\phi$  satisfies the Laplace equation

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2} = 0$$

for 2-dimensional rotation or irrotational flow of incompressible fluids, a scalar function  $\psi(x, y, t)$  can be defined such that



$$-\frac{\partial \psi}{\partial y} = u + \frac{\partial \psi}{\partial y} = v$$

for irrotational flow  $\psi$  satisfies

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = 0$$

$$\text{i.e. } \nabla^2 \psi = 2\omega_z$$

### 1.2.7 Laminar Flow

For Newtonian fluids, flow can be classified as laminar or turbulent,

depending on Reynolds number  $R = \frac{\rho v l}{\mu}$

Where  $l$  is the characteristic length,  $\rho$  is the density of the fluid,  $v$  is the velocity of the flow and  $\mu$  is the viscosity.

The characteristics of laminas flow are

1. No slip at the boundary that is because viscosity velocity of fluid at  $y = 0$

If boundary is stationary or if equal to the velocity of the boundary if it is in motion.

2. Because of viscosity there is shear between fluid layer which is given by

$$\Gamma = \mu \frac{du}{dy} \text{ for flow in the } u - \text{direction}$$

3. Flow is rotational
  4. There is continuous dissipation of energy due to uncoil shear and energy must be supplied continuously to maintain the flow
  5. There is no mixing between different fluid layers except by molecular motion which is very small
  6. Flow remains laminar as long as Reynolds number is less than the critical value.
  7. Energy loss is proportional to first power of velocity and first power of viscosity.
- laminar flow occurs in capillary tubes, blood vessels, in the case of flow <sup>past</sup> ~~pan~~ tiny bodies like lubrication bearings, underground flow etc. characteristics 1, 3, 4 are true for turbulent flow.

## 2.8 Turbulent flows

As mentioned in laminar flow, when the Reynolds number exceeds the critical value, turbulent flow develops. Turbulent flows occur more often than in nature and in engineering applications than laminar flow. The characteristics of turbulent flow can be summarized as follows:-

1. No slip condition is satisfied at the boundary
2. Turbulence is generated due to instability of flow in region of high shear i.e. near the boundary or at the interface of two moving layers. The former is called wall turbulence while the latter is called free turbulence
3. Local velocity component, pressure, force or any other quality associated with flow

such as local concentration, of abetment show random fluctuation.

4. Vigorousness of turbulent at any given point is measured by turbulence intensity
5. Turbulent flow is characterize by the presence of circulation fluid mass known as eddies.
6. Presence of eddies is the flow maker it capable of efficient transport momentum, mass or energy across the flow.
7. Presence of turbulence fluctuations in velocities causes additional normal and tangential Stresses at any point.

#### **1.2.9. Transition from laminar to turbulence Flow**

Laminar flow takes place only at small values of Reynolds number. For pipe flow Reynolds number must be less than 2100; for open channel flow, Reynolds number must be less than 500. The Reynolds number at which flow cease to be laminar is known as critical Reynolds number.

## CHAPTER TWO

### MATHEMATICAL REVIEW

#### 2.0 INTRODUCTION

In this chapter, we shall proceed to give a mathematical review of vectors, Divergence of a Vector and the curl of a Vector. We shall also give the Divergence and curl of a Vector in spherical coordinates.

A Vector is a quantity which possesses both magnitude and direction and is normally denoted by bold lower case letters or a line segment such as  $\vec{a}$  or

$$A\vec{B} \text{ where } \vec{a} = a_1i + a_2j + a_3k \dots\dots\dots 2.1.0$$

#### 2.1 GRADIENT, DIVERGENCE AND CURL

Consider the Vector operator  $\nabla$  (del) defined by

$$\nabla = i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z} \dots\dots\dots 2.1.1$$

Then if  $\Phi(x,y,z)$  and  $A(x,y,z)$  have continuous partial derivatives in a region, we can define the following

2.1.0 Gradient: The Gradient of  $\Phi$  is defined by

$$\begin{aligned} \text{Grad } \Phi = \nabla\Phi &= \left(i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z}\right)\Phi \\ &= i \frac{\partial\Phi}{\partial x} + j \frac{\partial\Phi}{\partial y} + k \frac{\partial\Phi}{\partial z} \dots\dots\dots 2.1.2 \end{aligned}$$

An interesting interpretation is that if  $\Phi(x, y, z) = c$

is the equation of a surface, then  $\nabla\Phi$  is a normal to the surface.

2.1.1 **DIVERGENCE** The divergence of **A** is defined by

$$\begin{aligned} \text{divA} = \nabla \cdot A &= \left(i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z}\right) \cdot (A_1i + A_2j + A_3k) \\ &= \frac{\partial A_1}{\partial x} + \frac{\partial A_2}{\partial y} + \frac{\partial A_3}{\partial z} \dots\dots\dots 2.1.3 \end{aligned}$$

2.1.2 **CURL** The curl of **A** is defined by

$$\text{Curl A} = \nabla \times A$$

$$= \left(i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z}\right) \times (A_1i + A_2j + A_3k)$$

$$= \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_1 & A_2 & A_3 \end{vmatrix}$$

$$= i \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial z} \\ A_2 & A_3 \end{vmatrix} - j \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial z} \\ A_1 & A_3 \end{vmatrix} + k \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ A_1 & A_2 \end{vmatrix}$$

$$= \left( \frac{\partial A_3}{\partial y} - \frac{\partial A_2}{\partial z} \right) i - \left( \frac{\partial A_3}{\partial x} - \frac{\partial A_1}{\partial z} \right) j + \left( \frac{\partial A_2}{\partial x} - \frac{\partial A_1}{\partial y} \right) k \dots\dots\dots 2.1.4$$

2.1.3 Examples: If  $\Phi = x^2 yz^3$  and  $A = xzi - y^2 j + 2x^2 yk$

find the following:

- (a)  $\nabla \Phi$
- (b)  $\nabla \cdot A$
- (c)  $\nabla \times A$
- (d)  $\nabla \cdot (\Phi A)$
- (e)  $\nabla \times (\Phi A)$

Solutions:

$$\begin{aligned}(a) \quad \nabla \Phi &= \left( i \frac{\partial}{\partial x} + j \frac{\partial}{\partial y} + k \frac{\partial}{\partial z} \right) \Phi \\ &= i \frac{\partial \Phi}{\partial x} + j \frac{\partial \Phi}{\partial y} + k \frac{\partial \Phi}{\partial z} \\ &= i \frac{\partial}{\partial x} (x^2 y z^3) + j \frac{\partial}{\partial y} (x^2 y z^3) + k \frac{\partial}{\partial z} (x^2 y z^3) \\ &= 2xyz^3 i + x^2 z^3 j + 3x^2 y z^2 k\end{aligned}$$

$$\begin{aligned}(b) \quad \nabla \cdot A &= \left( \frac{\partial}{\partial x} i + \frac{\partial}{\partial y} j + \frac{\partial}{\partial z} k \right) (xzi - y^2 j + 2x^2 y k) \\ &= \frac{\partial}{\partial x} (xz) + \frac{\partial}{\partial y} (-y^2) + \frac{\partial}{\partial z} (2x^2 y) \\ &= z - 2y\end{aligned}$$

$$\begin{aligned}
(c) \quad \nabla XA &= \left( \frac{\partial}{\partial x} i + \frac{\partial}{\partial y} j + \frac{\partial}{\partial z} k \right) X(xzi - y^2 j + 2x^2 yk) \\
&= \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ xz & -y^2 & 2x^2 y \end{vmatrix} \\
&= i \begin{vmatrix} \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -y^2 & 2x^2 y \end{vmatrix} - j \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial z} \\ xy & 2x^2 y \end{vmatrix} + k \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ xz & -y^2 \end{vmatrix} \\
&= i \left[ \frac{\partial(2x^2 y)}{\partial y} - \frac{\partial(-y)}{\partial z} \right] - j \left[ \frac{\partial(2x^2 y)}{\partial x} - \frac{\partial(xy)}{\partial z} \right] + k \left[ \frac{\partial(-y^2)}{\partial x} - \frac{\partial(xz)}{\partial y} \right] \\
&= 2x^2 i - (x - 4xy) j
\end{aligned}$$

$$\begin{aligned}
(d) \quad \nabla \cdot (\Phi A) &= \nabla \cdot [x^2 y z^3 (xzi - y^2 j + 2x^2 yk)] \\
&= \nabla \cdot (x^3 y z i - x^2 y^3 z^3 j + 2x^4 y^2 z^3 k) \\
&= 3x^2 y z^4 - 3x^2 y^2 z^3 + 6x^4 y^2 z^2
\end{aligned}$$



$$(e) \nabla \times (\phi A) = \nabla \times (x^3 y z^4 i - x^2 y z^3 j + 2x^4 y^2 z^3 k)$$

$$\begin{aligned}
 &= \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ x^3 y^3 z^3 & -x^2 y^3 z^3 & 2x^4 y^2 z^3 \end{vmatrix} \\
 &= i \begin{vmatrix} \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -x^2 y^3 z^3 & 2x^4 y^2 z^3 \end{vmatrix} - j \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial z} \\ x^3 y z^4 & 2x^4 y^2 z^3 \end{vmatrix} \\
 &\quad + k \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ x^3 y z^4 & -x^2 y^3 z^3 \end{vmatrix} \\
 &= i \left[ \frac{\partial}{\partial y} (2x^4 y^2 z^3) - \frac{\partial}{\partial z} (-x^2 y^3 z^3) \right] - j \left[ \frac{\partial}{\partial x} (2x^4 y^2 z^3) - \frac{\partial}{\partial z} (x^3 y z^4) \right] \\
 &\quad + k \left[ \frac{\partial}{\partial x} (-x^2 y^3 z^3) - \frac{\partial}{\partial y} (x^3 y z^4) \right] \\
 &= (4x^4 y z^3 + 3x^2 y^3 z^2) i + (4x^3 y z^3 - 8x^3 y^2 z^3) j - (-2xy^3 z^3 - x^3 z^4) \\
 &\quad + (-2xy^3 z^3 - x^3 z^4) k
 \end{aligned}$$

## 2.2 ORTHOGONAL CURVILINEAR COORDINATES

The transformation equation

$$\begin{aligned}
 x &= f(u_1, u_2, u_3), \\
 y &= g(u_1, u_2, u_3) \dots \dots \dots 2.2.1 \\
 z &= h(u_1, u_2, u_3)
 \end{aligned}$$

establish a one-to-one correspondence between points  $u_1, u_2, u_3$  in  $x, y, z$  and rectangular coordinate system.

In vector notation, the transformation (2.2.1) can be written as

$$\begin{aligned} r &= xi + yj + zk \\ &= f(u_1, u_2, u_3)i + g(u_1, u_2, u_3)j + h(u_1, u_2, u_3)k \dots\dots 2.2.2 \end{aligned}$$

A point P in space can then be defined not only by rectangular coordinates  $(x, y, z)$  but by the coordinates  $(u_1, u_2, u_3)$  as well. We call  $(u_1, u_2, u_3)$  the curvilinear coordinates of the point.

From (2.2.2)

$$dr = \frac{\partial r}{\partial u_1} du_1 + \frac{\partial r}{\partial u_2} du_2 + \frac{\partial r}{\partial u_3} du_3 \dots\dots 2.2.3$$

The vector  $\frac{\partial r}{\partial u_1}$  is tangent to the  $u_1$  coordinate curve at P. If  $e_1$  is a unit vector

at p in this direction, we can write  $h_1 = \left| \frac{\partial r}{\partial u_1} \right|$

where  $h_1 = \left| \frac{\partial r}{\partial u_1} \right|$ .

Similarly we can write

$$\frac{\partial r}{\partial u_2} = h_2 e_2 \quad \text{and} \quad \frac{\partial r}{\partial u_3} = h_3 e_3$$

where  $h_2 = \left| \frac{\partial r}{\partial u_2} \right|$  and  $h_3 = \left| \frac{\partial r}{\partial u_3} \right|$  respectively.

Therefore (2.2.3) becomes

$$dr = h_1 du_1 e_1 + h_2 du_2 + h_3 du_3 \dots \dots \dots 2.2.4$$

where  $h_1, h_2, h_3$  are scale factors.

If  $e_1, e_2, e_3$  are mutually perpendicular at P, then the curvilinear coordinates are called orthogonal.

Therefore the element of length  $ds$  is given by

$$\begin{aligned} ds^2 &= dr \cdot dr \\ &= h_1^2 du_1^2 + h_2^2 du_2^2 + h_3^2 du_3^2 \dots \dots \dots 2.2.5 \end{aligned}$$

and corresponds to the square of the length of the diagonal in a parallelepiped.

Also the volume of the parallelepiped is given by

$$\begin{aligned} dv &= |(h_1 du_1 e_1) \cdot (h_2 du_2 e_2) \cdot (h_3 du_3 e_3)| \\ &= h_1 h_2 h_3 du_1 du_2 du_3 \dots \dots \dots 2.2.6 \end{aligned}$$

$$\begin{aligned} &= \left| \frac{\partial r}{\partial u_1} \cdot \frac{\partial r}{\partial u_2} \times \frac{\partial r}{\partial u_3} \right| du_1 du_2 du_3 \\ &= \left| \frac{\partial(x, y, z)}{\partial(u_1, u_2, u_3)} \right| du_1 du_2 du_3 \dots \dots \dots 2.2.7 \end{aligned}$$

where  $\frac{\partial(x, y, z)}{\partial(u_1, u_2, u_3)}$  is the Jacobian of the transformation.

### 2.2.1 GRADIENT, DIVERGENCE, CURL AND LAPLACIAN IN ORTHOGONAL CURVILINEAR COORDINATES

If  $\Phi$  is a scalar function and  $A = A_1 e_1 + A_2 e_2 + A_3 e_3$  a vector function of orthogonal curvilinear coordinates  $u_1, u_2, u_3$  we have the following results

$$(i) \quad \nabla \Phi = \frac{1}{h_1} \frac{\partial \Phi}{\partial u_1} e_1 + \frac{1}{h_2} \frac{\partial \Phi}{\partial u_2} e_2 + \frac{1}{h_3} \frac{\partial \Phi}{\partial u_3} e_3$$

$$(ii) \quad \nabla \cdot A = \frac{1}{h_1 h_2 h_3} \left\{ \frac{\partial}{\partial u_1} (h_2 h_3 A_1) + \frac{\partial}{\partial u_2} (h_3 h_1 A_2) + \frac{\partial}{\partial u_3} (h_1 h_2 A_3) \right\}$$

$$(iii) \quad \nabla \times A = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} h_1 e_1 & h_2 e_2 & h_3 e_3 \\ \frac{\partial}{\partial u_1} & \frac{\partial}{\partial u_2} & \frac{\partial}{\partial u_3} \\ h_1 A_1 & h_2 A_2 & h_3 A_3 \end{vmatrix}$$

$$(iv) \quad \nabla^2 \Phi = \frac{1}{h_1 h_2 h_3} \left\{ \frac{\partial}{\partial u_1} \left( \frac{h_2 h_3}{h_1} \frac{\partial \Phi}{\partial u_1} \right) + \frac{\partial}{\partial u_2} \left( \frac{h_3 h_1}{h_2} \frac{\partial \Phi}{\partial u_2} \right) + \frac{\partial}{\partial u_3} \left( \frac{h_1 h_2}{h_3} \frac{\partial \Phi}{\partial u_3} \right) \right\}$$

These reduce to the usual expressions in rectangular coordinates if we

replace  $(u_1, u_2, u_3)$  by  $(x, y, z)$  in which case  $e_1, e_2, e_3$  are replaced by  $i, j$  and  $k$  and  $h_1 = h_2 = h_3 = 1$

## 2.2.2 SPHERICAL COORDINATES

Given the spherical coordinates  $(r, \theta, \phi)$  the transformation equation is given by

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

$$\text{where } r \geq 0, 0 \leq \theta \leq \pi, 0 \leq \phi \leq 2\pi$$

Scale factor  $h_1 = 1, h_2 = r, h_3 = r \sin \theta$

Element of arc length  $ds^2$  is given by

$$ds^2 = dr^2 + r^2 d\theta^2 + r^2 \sin^2 \theta d\phi^2$$

Jacobian  $\frac{\partial(x, y, z)}{\partial(r, \theta, \phi)} = r^2 \sin \theta$

element of volume  $dr = r^2 \sin \theta dr d\theta d\phi$

Laplacian:

$$\nabla^2 U = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial U}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial U}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 U}{\partial \phi^2}$$

## 2.3 LEGENDRE FUNCTION

### 2.3.1 LEGENDRE DIFFERENTIAL EQUATION

The Legendre's functions arises as solutions of the differential equations

$$(1 - x^2)y'' - 2xy' + n(n+1)y = 0 \dots\dots\dots 2.3.1$$

which is called the Legendre differential equation.

The general solution of (2.3.1) in the case when  $n=0, 1, 2, 3, \dots$  is given by;

$$y = c_1 P_n(x) + c_2 Q_n(x)$$

where  $P_n(x)$  are polynomials called Legendre polynomials and  $Q_n(x)$  are

called Legendre functions of the second kind which are unbounded at

$$x = \pm 1$$

### 2.3.2 LEGENDRE POLYNOMIALS

The Legendre polynomials are defined by

$$P_n = \frac{(2n-1)(2n-3)\dots\dots 1}{n!} \left\{ x^n - \frac{n(n-1)x^{n-2}}{2(n-1)} + \frac{n(n-1)(n-2)(n-3)x^{n-4}}{2.4.(2n-1)(2n-3)\dots\dots} - \dots\dots \right\} \dots\dots\dots 2.3.2$$

where  $P_n$  is a polynomial of degree  $n$

The Legendre polynomial can also be expressed as

$$P_n(x) = \frac{1}{2^n n!} \frac{d^n}{dx^n} (x^2 - 1)^n \dots\dots\dots 2.3.3$$

### 2.3.3 ASSOCIATED LEGENDRE FUNCTIONS

The differential equation

$$(1 - x^2)y'' - 2xy' + \left\{ n(n+1) - \frac{m^2}{1-x^2} \right\} y = 0 \dots\dots\dots 2.3.4$$

Is called Legendre's associated differential equation. If  $m=0$ , this reduce to Legendre's equation. Solution to (2.3.4) are called associated Legendre's functions.

### 2.4 Problem Formulation

In this section we shall proceed to given a brief formulation of the problem of the flow of fluid past a sphere.

Let  $a$  be the radius of the sphere and  $U$  be the speed of the uniform streaming motion at in infinity assumed to be parallel to the positive  $x$ -axis of a system of coordinates based on the center of the sphere. The velocity field  $UV$  and the space coordinates can be non-dimensionalized with the aid of  $U$  and  $a$  respectively and the equations of the motion will then be

$$\nabla^2 U - \nabla p = R(V \cdot \nabla)V, \quad \nabla V = 0 \dots \dots \dots 2.4.1$$

Where  $\rho \nu U p/a$  is the pressure,  $R = Ua/\nu$  is the Reynolds number,  $\rho$  is the density and  $\nu$  is the kinematic viscosity.

Neglecting the inertia terms in the absence of extraneous forces, the equation is in the form

$$\mu \nabla^2 U = \frac{\partial p}{\partial x} \dots \dots \dots 2.4.2$$



**CHAPTER THREE**  
**SOLUTION OF PROBLEM**

**3.0 METHOD OF SOLUTION**

Considering the equation (2.4.2)

$$\mu \nabla^2 U = \frac{\partial P}{\partial x} \dots\dots\dots 3.0.1$$

Which can be rewritten as

$$\mu \nabla^2 U = \frac{\partial p}{\partial u} \cdot \frac{\partial u}{\partial x} \dots\dots\dots 3.0.2$$

Taking  $\varepsilon = \frac{\partial p}{\partial u}$ , we have

$$\mu \nabla^2 U = \varepsilon \frac{\partial u}{\partial x} \dots\dots\dots 3.0.3$$

Where  $\varepsilon$  is the perturbation parameter.

we shall now proceed to expand U in terms of  $\varepsilon$ , we have

$$U = \varepsilon^0 U_0 + \varepsilon^1 U_1 + \varepsilon^2 U_2 + \varepsilon^3 U_3 + \dots \quad 3.0.4$$

Putting (3.0.4) into (3.0.3) we have

$$\begin{aligned} \varepsilon^0 \mu \nabla^2 U_0 + \varepsilon^1 \mu \nabla^2 U_1 + \varepsilon^2 \mu \nabla^2 U_2 + \dots \\ = \varepsilon^1 \frac{\partial u_0}{\partial x} + \varepsilon^2 \frac{\partial u_1}{\partial x} + \varepsilon^3 \frac{\partial u_2}{\partial x} + \dots \end{aligned} \quad 3.0.5$$

Rearranging (3.0.5) in terms of order  $\varepsilon$ , we have

$$\begin{aligned} \varepsilon^0; \mu \nabla^2 U_0 &= 0 \\ \varepsilon^1; \mu \nabla^2 U_1 &= \frac{\partial U_0}{\partial x} \\ \varepsilon^2; \mu \nabla^2 U_2 &= \frac{\partial U_1}{\partial x} \end{aligned}$$

and so on for higher order of  $\varepsilon$

### 3.1. SOLUTION OF ORDER $\varepsilon^0$ EQUATION

We shall proceed to solve the order  $\varepsilon^0$  equation given by

$$\mu \nabla^2 U_0 = 0 \Rightarrow \nabla^2 U_0 = 0 \dots \dots \dots 3.1.0$$

Writing this order  $\varepsilon^0$  equation in spherical coordinates, we have;

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial U_0}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial U_0}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 U_0}{\partial \phi^2} \quad \checkmark$$

\dots \dots \dots 3.1.1

Our method of procedure will be as follows,

We try a solution of the form

$$U(r, \theta, \phi) = R(r)\Theta(\theta)\Phi(\phi) \dots \dots \dots 3.1.2$$

Substituting this into (3.1.1) and dividing through by  $U = R\Theta\Phi$  and multiplying by  $r^2$ , we have

$$\frac{1}{R} \frac{\partial}{\partial r} \left( r^2 \frac{\partial R}{\partial r} \right) + \frac{1}{\Theta \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial \Theta}{\partial \theta} \right) + \frac{1}{\Phi \sin^2 \theta} \frac{\partial^2 \Phi}{\partial \phi^2} \dots \dots \dots 3.1.3$$

The first term depends only on  $r$  and the second (3.1.1) and third term (taken together) only on  $\theta$  and  $\phi$  (3.1.3) can be written as

$$\frac{1}{R} \frac{d}{dr} \left( r^2 \frac{dR}{dr} \right) = \lambda \dots \dots \dots 3.1.4$$

and

$$\frac{1}{\Theta \sin \theta} \frac{d}{d\theta} \left( \sin \theta \frac{d\Theta}{d\theta} \right) + \frac{1}{\Phi \sin^2 \theta} \frac{d^2 \Phi}{d\phi^2} = -\lambda \dots \dots \dots 3.15$$

from (3.1.4)

$$\Rightarrow \frac{1}{R} \left[ 2r \frac{dR}{dr} + r^2 \frac{d^2 R}{dr^2} \right] = \lambda$$

Therefore,

$$2r \frac{dR}{dr} + r^2 \frac{d^2 R}{dr^2} = \lambda R$$

$$\Rightarrow r^2 \frac{d^2 R}{dr^2} + 2r \frac{dR}{dr} - \lambda R = 0 \dots \dots \dots 3.16$$

(3.1.6) can be reduced by substitution

$$r = \exp t (r = e^t)$$

and writing  $R(r) = S(t)$  to

$$\frac{d^2 S}{dt^2} + \frac{dS}{dt} - \lambda S = 0$$

This has the solution

$$S(t) = Ar^{\lambda_1 t} + Br^{\lambda_2 t}$$

Therefore the solution to the radial equation is

$$R(r) = Ar^{\lambda_1} + Br^{\lambda_2}$$

Where  $\lambda_1 + \lambda_2 = -1$ , and  $\lambda_1\lambda_2 = -\lambda$  and we can take  $\lambda_1$  and  $\lambda_2$  as given by  $l$  and  $-(l+1)$

$\lambda$  then has the form  $l(l+1)$

Hence we have the separated variable solution, which will have the form

$$U(r, \theta, \phi) = (Ar^l + Br^{-(l+1)})\Theta(\theta)\Phi(\phi) \dots \dots \dots 3.1.7$$

Where  $\Theta$  and  $\Phi$  must satisfy (3.1.5) with  $\lambda = l(l+1)$

Multiplying (3.1.5) through by  $\sin^2\theta$  and substituting for  $\lambda$ ,

It takes a separated form.

$$\left[ \frac{\sin\theta}{\Theta} \frac{d}{d\theta} \left( \sin\theta \frac{d\Theta}{d\theta} \right) + l(l+1)\sin^2\theta \right] + \frac{1}{\Phi} \frac{d^2\Phi}{d\phi^2} = 0 \dots \dots \dots 3.1.8$$

Taking the separation constant as  $m^2$ , the equation in the azimuthal angle  $\phi$  has the same solution as cylindrical polars.

$$\frac{1}{\Phi} \frac{d^2\Phi}{d\phi^2} = -m$$

$$\frac{d^2\Phi}{d\phi^2} = -m^2\Phi$$

$$\Phi(\phi) = C\cos m\phi + D\sin m\phi$$

For  $m = 0$ , we have  $\Phi(\phi) = C$

Having settled the form of  $\Phi(\phi)$ , we are left only with the equation satisfied by  $\Theta(\theta)$ , which is

$$\frac{\sin\theta}{\Theta} \frac{d}{d\theta} \left[ \sin\theta \frac{d\Theta}{d\theta} \right] + l(l+1)\sin^2\theta = m^2 \dots\dots\dots 3.1.9$$

A change of independent variable from  $\theta$  to  $z = \cos\theta$ , will reduce this to a form, from which solutions are known.

Putting  $z = \cos\theta$ ,  $\frac{dz}{d\theta} = -\sin\theta$ ,  $\frac{d}{d\theta} = -(1-z^2)^{1/2} \frac{d}{dz}$

The equation for  $M(z) \equiv \Theta(\theta)$  reads;

$$\frac{d}{dz} \left[ (1-z^2) \frac{dM}{dz} \right] + \left[ l(l+1) - \frac{m^2}{1-z^2} \right] M = 0 \dots\dots\dots 3.1.10$$

This equation is the associated Legendre equation.

From (3.1.10),

$$\Rightarrow (1-z^2) \frac{d^2 M}{dz^2} - 2z \frac{dM}{dz} + \left[ l(l+1) - \frac{m^2}{1-z^2} \right] M = 0$$

For  $m = 0$ , we have

$$(1-z^2) \frac{d^2 M}{dz^2} - 2z \frac{dM}{dz} + l(l+1)M = 0 \dots\dots\dots 3.1.11$$

(3.1.11) is the Legendre's equation which we shall proceed to solve using series solution method

method.

Assuming a solution of the form

$$M(z) = \sum_{n=0}^{\infty} a_n z^n$$

then

$$\frac{dM}{dz} = \sum_{n=0}^{\infty} n a_n z^{n-1}$$

$$\frac{d^2 M}{dz^2} = \sum_{n=0}^{\infty} n(n-1) a_n z^{n-2}$$

Substituting into (3.1.11), we have

$$\sum_{n=0}^{\infty} [n(n-1)a_n Z^{n-2} - n(n-1)a_n Z^n - 2na_n Z^n + l(l+1)a_n Z^n] = 0$$

which on collecting terms gives

$$\sum_{n=0}^{\infty} [(n+2)(n+1)a_{n+2} - [n(n+1) - l(l+1)]a_n] Z^n = 0$$

The recurrence relation is therefore

$$a_{n+2} = \frac{[n(n+1) - l(l+1)]a_n}{(n+1)(n+2)}$$

For  $n=0,1,2,3\dots$

When  $n = 0$ , we have

$$a_2 = \frac{-l(l+1)}{2} a_0$$

When  $n = 1$ , we have

$$a_3 = \frac{[2 - l(l+1)]}{2(3)} a_0$$

Choosing  $a_0 = 1$  and  $a_1 = 0$ , we have

$$M_1(z) = 1 - \frac{l(l+1)}{2!} z^2 + \frac{(l-2)l(l+1)(l+3)}{4!} z^4 \dots\dots\dots 3.1.12$$

choosing  $a_0 = 0$  and  $a_1 = 1$ , we have

$$M_2(z) = z - \frac{(l-1)(l+2)}{3!} z^3 + \frac{(l-3)(l-1)(l+2)(l+4)}{5!} z^5 \dots\dots\dots 3.1.13$$



Since (3.1.12) contains only even powers of  $z$  and (3.1.13) contains only odd powers, these two solutions cannot be proportional to one another and are therefore linearly independent.

Hence

$$M(z) = EM_1(z) + FM_2(z)$$

is the general solution to (3.1.10).

But for general  $M$ ,  $M_1(z)$  and  $M_2(z)$  are the associated Legendre function, which can be written as  $P_l^m(z)$  and  $Q_l^m(z)$ .

Therefore,  $M_l^m(z) = EP_l^m(z) + FQ_l^m(z)$

Now that the solution of each of the three ordinary differential equation

$R, \theta$  and  $\Phi$  have been obtained, we may assemble a complete separated variable solution in spherical polars. It is

$$U(r, \theta, \phi) = (Ar^l + Br^{-(l+1)})(C\cos m\phi + D\sin m\phi)[EP_l^m(\cos\theta) + FQ_l^m(\cos\theta)].$$

.....(3.1.14)

Since the flow is symmetric about the sphere, we have  $m = 0$ , therefore (3.1.14) becomes

$$U(r, \theta, \phi) = Ar^l + Br^{-(l+1)}(C)[EP_l(\cos\theta) + FQ_l(\cos\theta)].....(3.1.15)$$

Since  $Q_l$  denotes an infinite series, which can exist mathematically but is invariably unreasonable on physical ground, because the solution is expected to be finite, it cannot contain  $Q_l$

Therefore 3.1.15 becomes

$$U(r, \theta) = \sum_{l=0}^{\infty} [A_l r^l + B_l r^{-(l+1)}] [P_l(\cos \theta)] \dots\dots\dots 3.1.16$$

(3.1.16) is the general form of the solution.

Using the boundary condition at  $r = \infty$ ,  $U = 0$

$$A_l = 0$$

We have  $\Rightarrow U(r, \theta) = \sum_{l=0}^{\infty} B_l r^{-(l+1)} [P_l(\cos \theta)] \dots\dots\dots 3.1.17$

Using the boundary condition  $r = a$ ,  $U = U_0$  we have

$$U(a, \theta) = \sum_{l=0}^{\infty} B_l a^{-(l+1)} [P_l(\cos \theta)] \dots\dots\dots 3.1.18$$

$$U(a, \theta) = U_0$$

We shall now obtain the value of  $B_l$ . Using the mutual orthogonality of Legendre Polynomials

We have

$$B_l a^{-(l+1)} = \frac{2l+1}{2} U_0 \int_0^1 P_l(z) dz \quad \text{where } z = \cos \theta$$

Therefore

$$B_l a^{l+1} = \frac{2l+1}{2} U_0 \int_0^1 P_l(z) dz \quad \text{from 3.1.17}$$

$\Rightarrow$  the solution required will become

$$U(r, \theta) = \sum_{l=0}^{\infty} a^{l+1} \frac{2l+1}{2} U_0 \int_0^1 P_l(z) dz \cdot r^{-(l+1)} [P_l(\cos \theta)]$$

$$U(r, \theta) = \frac{U_0 a}{2r} \left[ 1 + \frac{3a}{2r} P_1(\cos \theta) - \frac{7a^3}{8r^3} P_3(\cos \theta) + \dots \right] \dots \dots (3.1.19)$$

## CHAPTER FOUR NUMERICAL RESULTS

Considering the solution of the order  $\varepsilon^0$  equation then

$$U(r, \theta) = \sum_{l=0}^{\infty} a^{(l+1)} \frac{2l+1}{2} U_0 \int_0^1 P_l(z) dz \cdot r^{-(l+1)} [P_l(\cos \theta)]$$

$$U(r, \theta) = \frac{U_0 a}{2r} \left[ 1 + \frac{3a}{2r} P_1(\cos \theta) - \frac{7a^3}{8r^3} P_3(\cos \theta) + \dots \right] \quad 4.0.1$$

We proceed to analyse the above solution using **MATHCAD**. The tables and graphs in the subsequent pages shows the different values of

$U(r, \theta)$  against  $\theta$  for  $\frac{a}{r} = \mu$  taken as a constant.

The equation 4.0.1 is written in MATHCAD as follows:

b:=0 c:=10 d:=360

b:=b.deg c:=c.deg D:=d.deg

$U_0 := 0.1$   $\mu_1 := 0.1, 0.11, 0.2$   $\theta := b, c, d$   $B := 0, 10, 360$

$$U_1(\theta, \mu_1) := \frac{U_0}{2} \cdot \mu_1 \cdot \left[ 1 + \frac{3}{2} \cdot \mu_1 - \frac{3}{2} \cdot \mu_1 \cdot \left( \sin\left(\frac{1}{2} \cdot \theta\right) \right)^2 - \frac{7}{8} \cdot \mu_1^3 \dots \right. \\ \left. + 84 \cdot \mu_1^3 \cdot \left( \sin\left(\frac{1}{2} \cdot \theta\right) \right)^2 - \frac{210}{8} \cdot \mu_1^3 \cdot \left( \sin\left(\frac{1}{2} \cdot \theta\right) \right)^4 \right]$$

**Table 4.1 Flow distribution for values of  $a/r = 0.1$  to  $0.14$**

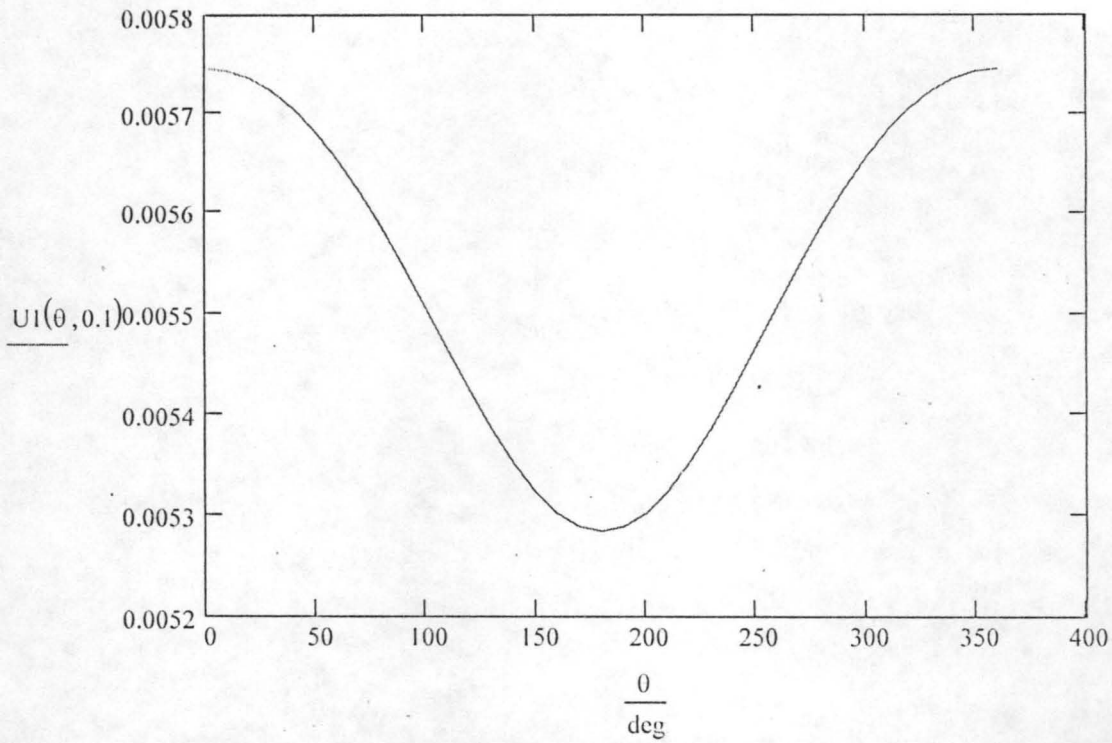
$\theta =$	$U_1(\theta, 0.1) = U_1(\theta, 0.11) = U_1(\theta, 0.12) = U_1(\theta, 0.13) = U_1(\theta, 0.14) =$				
deg					
0	5.746·10 <sup>-3</sup>	6.401·10 <sup>-3</sup>	7.071·10 <sup>-3</sup>	7.755·10 <sup>-3</sup>	8.453·10 <sup>-3</sup>
10	5.743·10 <sup>-3</sup>	6.399·10 <sup>-3</sup>	7.069·10 <sup>-3</sup>	7.754·10 <sup>-3</sup>	8.454·10 <sup>-3</sup>
20	5.736·10 <sup>-3</sup>	6.392·10 <sup>-3</sup>	7.064·10 <sup>-3</sup>	7.753·10 <sup>-3</sup>	8.457·10 <sup>-3</sup>
30	5.723·10 <sup>-3</sup>	6.381·10 <sup>-3</sup>	7.056·10 <sup>-3</sup>	7.749·10 <sup>-3</sup>	8.461·10 <sup>-3</sup>
40	5.705·10 <sup>-3</sup>	6.364·10 <sup>-3</sup>	7.043·10 <sup>-3</sup>	7.742·10 <sup>-3</sup>	8.463·10 <sup>-3</sup>
50	5.682·10 <sup>-3</sup>	6.343·10 <sup>-3</sup>	7.025·10 <sup>-3</sup>	7.731·10 <sup>-3</sup>	8.463·10 <sup>-3</sup>
60	5.655·10 <sup>-3</sup>	6.316·10 <sup>-3</sup>	7.002·10 <sup>-3</sup>	7.715·10 <sup>-3</sup>	8.458·10 <sup>-3</sup>
70	5.623·10 <sup>-3</sup>	6.284·10 <sup>-3</sup>	6.973·10 <sup>-3</sup>	7.692·10 <sup>-3</sup>	8.446·10 <sup>-3</sup>
80	5.587·10 <sup>-3</sup>	6.247·10 <sup>-3</sup>	6.938·10 <sup>-3</sup>	7.663·10 <sup>-3</sup>	8.426·10 <sup>-3</sup>
90	5.548·10 <sup>-3</sup>	6.207·10 <sup>-3</sup>	6.898·10 <sup>-3</sup>	7.627·10 <sup>-3</sup>	8.399·10 <sup>-3</sup>
100	5.507·10 <sup>-3</sup>	6.163·10 <sup>-3</sup>	6.855·10 <sup>-3</sup>	7.586·10 <sup>-3</sup>	8.364·10 <sup>-3</sup>
110	5.465·10 <sup>-3</sup>	6.118·10 <sup>-3</sup>	6.808·10 <sup>-3</sup>	7.541·10 <sup>-3</sup>	8.322·10 <sup>-3</sup>
120	5.424·10 <sup>-3</sup>	6.074·10 <sup>-3</sup>	6.761·10 <sup>-3</sup>	7.493·10 <sup>-3</sup>	8.277·10 <sup>-3</sup>
130	5.386·10 <sup>-3</sup>	6.031·10 <sup>-3</sup>	6.716·10 <sup>-3</sup>	7.446·10 <sup>-3</sup>	8.231·10 <sup>-3</sup>
140	5.352·10 <sup>-3</sup>	5.993·10 <sup>-3</sup>	6.674·10 <sup>-3</sup>	7.403·10 <sup>-3</sup>	8.187·10 <sup>-3</sup>
150	5.323·10 <sup>-3</sup>	5.961·10 <sup>-3</sup>	6.639·10 <sup>-3</sup>	7.365·10 <sup>-3</sup>	8.148·10 <sup>-3</sup>
160	5.302·10 <sup>-3</sup>	5.937·10 <sup>-3</sup>	6.612·10 <sup>-3</sup>	7.337·10 <sup>-3</sup>	8.118·10 <sup>-3</sup>
170	5.289·10 <sup>-3</sup>	5.921·10 <sup>-3</sup>	6.595·10 <sup>-3</sup>	7.318·10 <sup>-3</sup>	8.099·10 <sup>-3</sup>
180	5.284·10 <sup>-3</sup>	5.916·10 <sup>-3</sup>	6.59·10 <sup>-3</sup>	7.312·10 <sup>-3</sup>	8.092·10 <sup>-3</sup>
190	5.289·10 <sup>-3</sup>	5.921·10 <sup>-3</sup>	6.595·10 <sup>-3</sup>	7.318·10 <sup>-3</sup>	8.099·10 <sup>-3</sup>
200	5.302·10 <sup>-3</sup>	5.937·10 <sup>-3</sup>	6.612·10 <sup>-3</sup>	7.337·10 <sup>-3</sup>	8.118·10 <sup>-3</sup>
210	5.323·10 <sup>-3</sup>	5.961·10 <sup>-3</sup>	6.639·10 <sup>-3</sup>	7.365·10 <sup>-3</sup>	8.148·10 <sup>-3</sup>
220	5.352·10 <sup>-3</sup>	5.993·10 <sup>-3</sup>	6.674·10 <sup>-3</sup>	7.403·10 <sup>-3</sup>	8.187·10 <sup>-3</sup>
230	5.386·10 <sup>-3</sup>	6.031·10 <sup>-3</sup>	6.716·10 <sup>-3</sup>	7.446·10 <sup>-3</sup>	8.231·10 <sup>-3</sup>
240	5.424·10 <sup>-3</sup>	6.074·10 <sup>-3</sup>	6.761·10 <sup>-3</sup>	7.493·10 <sup>-3</sup>	8.277·10 <sup>-3</sup>
250	5.465·10 <sup>-3</sup>	6.118·10 <sup>-3</sup>	6.808·10 <sup>-3</sup>	7.541·10 <sup>-3</sup>	8.322·10 <sup>-3</sup>
260	5.507·10 <sup>-3</sup>	6.163·10 <sup>-3</sup>	6.855·10 <sup>-3</sup>	7.586·10 <sup>-3</sup>	8.364·10 <sup>-3</sup>
270	5.548·10 <sup>-3</sup>	6.207·10 <sup>-3</sup>	6.898·10 <sup>-3</sup>	7.627·10 <sup>-3</sup>	8.399·10 <sup>-3</sup>
280	5.587·10 <sup>-3</sup>	6.247·10 <sup>-3</sup>	6.938·10 <sup>-3</sup>	7.663·10 <sup>-3</sup>	8.426·10 <sup>-3</sup>
290	5.623·10 <sup>-3</sup>	6.284·10 <sup>-3</sup>	6.973·10 <sup>-3</sup>	7.692·10 <sup>-3</sup>	8.446·10 <sup>-3</sup>
300	5.655·10 <sup>-3</sup>	6.316·10 <sup>-3</sup>	7.002·10 <sup>-3</sup>	7.715·10 <sup>-3</sup>	8.458·10 <sup>-3</sup>
310	5.682·10 <sup>-3</sup>	6.343·10 <sup>-3</sup>	7.025·10 <sup>-3</sup>	7.731·10 <sup>-3</sup>	8.463·10 <sup>-3</sup>
320	5.705·10 <sup>-3</sup>	6.364·10 <sup>-3</sup>	7.043·10 <sup>-3</sup>	7.742·10 <sup>-3</sup>	8.463·10 <sup>-3</sup>
330	5.723·10 <sup>-3</sup>	6.381·10 <sup>-3</sup>	7.056·10 <sup>-3</sup>	7.749·10 <sup>-3</sup>	8.461·10 <sup>-3</sup>
340	5.736·10 <sup>-3</sup>	6.392·10 <sup>-3</sup>	7.064·10 <sup>-3</sup>	7.753·10 <sup>-3</sup>	8.457·10 <sup>-3</sup>
350	5.743·10 <sup>-3</sup>	6.399·10 <sup>-3</sup>	7.069·10 <sup>-3</sup>	7.754·10 <sup>-3</sup>	8.454·10 <sup>-3</sup>
360	5.746·10 <sup>-3</sup>	6.401·10 <sup>-3</sup>	7.071·10 <sup>-3</sup>	7.755·10 <sup>-3</sup>	8.453·10 <sup>-3</sup>

**Table 4.2 Flow distribution for values of  $a/r = 0.15$  to  $0.2$**

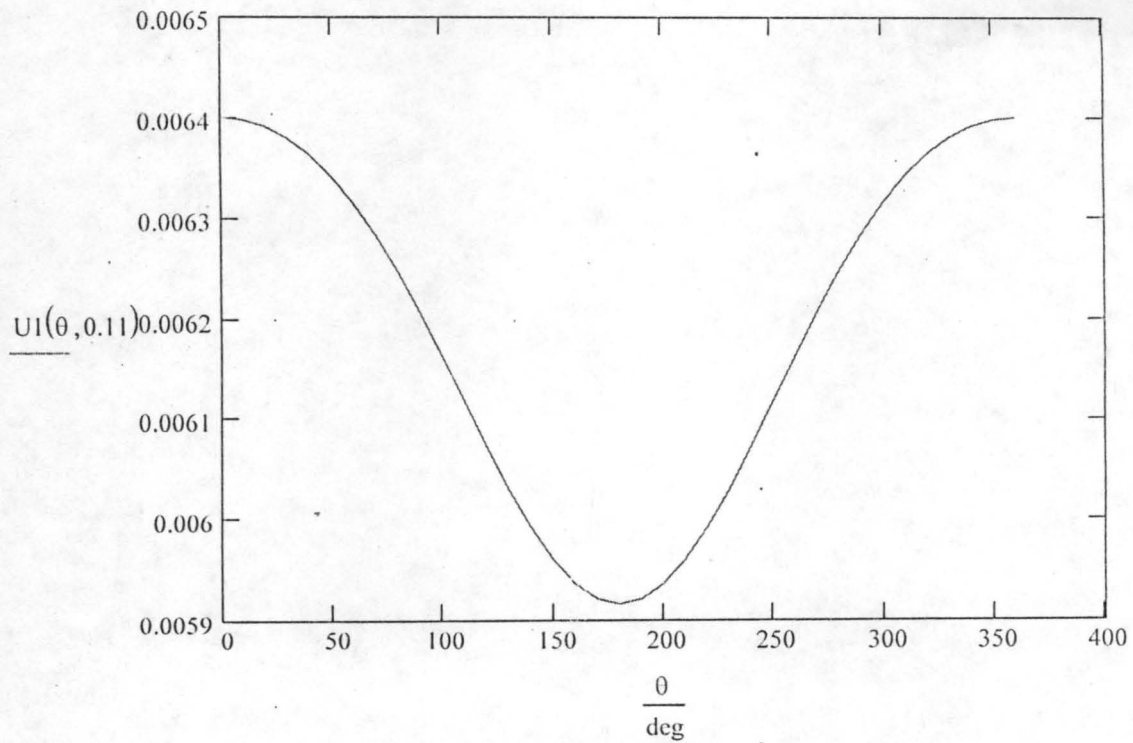
$\theta =$	$U1(\theta, 0.15)$	$U1(\theta, 0.16)$	$U1(\theta, 0.17)$	$U1(\theta, 0.18)$	$U1(\theta, 0.19)$	$U1(\theta, 0.2)$
0 deg	9.165·10 <sup>-3</sup>	9.891·10 <sup>-3</sup>	0.011	0.011	0.012	0.013
10	9.169·10 <sup>-3</sup>	9.898·10 <sup>-3</sup>	0.011	0.011	0.012	0.013
20	9.178·10 <sup>-3</sup>	9.916·10 <sup>-3</sup>	0.011	0.011	0.012	0.013
30	9.192·10 <sup>-3</sup>	9.943·10 <sup>-3</sup>	0.011	0.012	0.012	0.013
40	9.208·10 <sup>-3</sup>	9.977·10 <sup>-3</sup>	0.011	0.012	0.012	0.013
50	9.223·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
60	9.234·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
70	9.238·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
80	9.233·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
90	9.219·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
100	9.194·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
110	9.161·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
120	9.121·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.015
130	9.077·10 <sup>-3</sup>	9.995·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
140	9.035·10 <sup>-3</sup>	9.956·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
150	8.996·10 <sup>-3</sup>	9.919·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
160	8.966·10 <sup>-3</sup>	9.89·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
170	8.946·10 <sup>-3</sup>	9.87·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
180	8.94·10 <sup>-3</sup>	9.864·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
190	8.946·10 <sup>-3</sup>	9.87·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
200	8.966·10 <sup>-3</sup>	9.89·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
210	8.996·10 <sup>-3</sup>	9.919·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
220	9.035·10 <sup>-3</sup>	9.956·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
230	9.077·10 <sup>-3</sup>	9.995·10 <sup>-3</sup>	0.011	0.012	0.013	0.015
240	9.121·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.015
250	9.161·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
260	9.194·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
270	9.219·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
280	9.233·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
290	9.238·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
300	9.234·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
310	9.223·10 <sup>-3</sup>	0.01	0.011	0.012	0.013	0.014
320	9.208·10 <sup>-3</sup>	9.977·10 <sup>-3</sup>	0.011	0.012	0.012	0.013
330	9.192·10 <sup>-3</sup>	9.943·10 <sup>-3</sup>	0.011	0.012	0.012	0.013
340	9.178·10 <sup>-3</sup>	9.916·10 <sup>-3</sup>	0.011	0.011	0.012	0.013
350	9.169·10 <sup>-3</sup>	9.898·10 <sup>-3</sup>	0.011	0.011	0.012	0.013
360	9.165·10 <sup>-3</sup>	9.891·10 <sup>-3</sup>	0.011	0.011	0.012	0.013

**Table 4.3 Flow distribution for values of  $a/r = 0.3$  to  $1.0$**

$\theta =$	$U_1(\theta, 0.3) = U_1(\theta, 0.5) = U_1(\theta, 0.8) = U_1(\theta, 1) = U_1(\theta, 0.15)U_1(\theta, 0.2)$						
0	deg	0.021	0.041	0.07	0.081	0.012	0.013
10		0.022	0.043	0.083	0.113	0.012	0.013
20		0.022	0.048	0.12	0.204	0.012	0.013
30		0.023	0.057	0.18	0.352	0.012	0.013
40		0.024	0.068	0.258	0.546	0.012	0.013
50		0.026	0.082	0.352	0.776	0.013	0.014
60		0.028	0.097	0.455	1.03	0.013	0.014
70		0.029	0.112	0.562	1.296	0.013	0.014
80		0.031	0.128	0.669	1.562	0.013	0.014
90		0.032	0.142	0.772	1.816	0.013	0.014
100		0.034	0.156	0.866	2.05	0.013	0.014
110		0.035	0.168	0.95	2.258	0.013	0.014
120		0.036	0.178	1.022	2.437	0.013	0.015
130		0.037	0.186	1.081	2.584	0.013	0.015
140		0.037	0.192	1.128	2.7	0.013	0.015
150		0.038	0.197	1.162	2.787	0.013	0.015
160		0.038	0.2	1.186	2.847	0.013	0.015
170		0.038	0.202	1.2	2.882	0.013	0.015
180		0.038	0.203	1.205	2.894	0.013	0.015
190		0.038	0.202	1.2	2.882	0.013	0.015
200		0.038	0.2	1.186	2.847	0.013	0.015
210		0.038	0.197	1.162	2.787	0.013	0.015
220		0.037	0.192	1.128	2.7	0.013	0.015
230		0.037	0.186	1.081	2.584	0.013	0.015
240		0.036	0.178	1.022	2.437	0.013	0.015
250		0.035	0.168	0.95	2.258	0.013	0.014
260		0.034	0.156	0.866	2.05	0.013	0.014
270		0.032	0.142	0.772	1.816	0.013	0.014
280		0.031	0.128	0.669	1.562	0.013	0.014
290		0.029	0.112	0.562	1.296	0.013	0.014
300		0.028	0.097	0.455	1.03	0.013	0.014
310		0.026	0.082	0.352	0.776	0.013	0.014
320		0.024	0.068	0.258	0.546	0.012	0.013
330		0.023	0.057	0.18	0.352	0.012	0.013
340		0.022	0.048	0.12	0.204	0.012	0.013
350		0.022	0.043	0.083	0.113	0.012	0.013
360		0.021	0.041	0.07	0.081	0.012	0.013

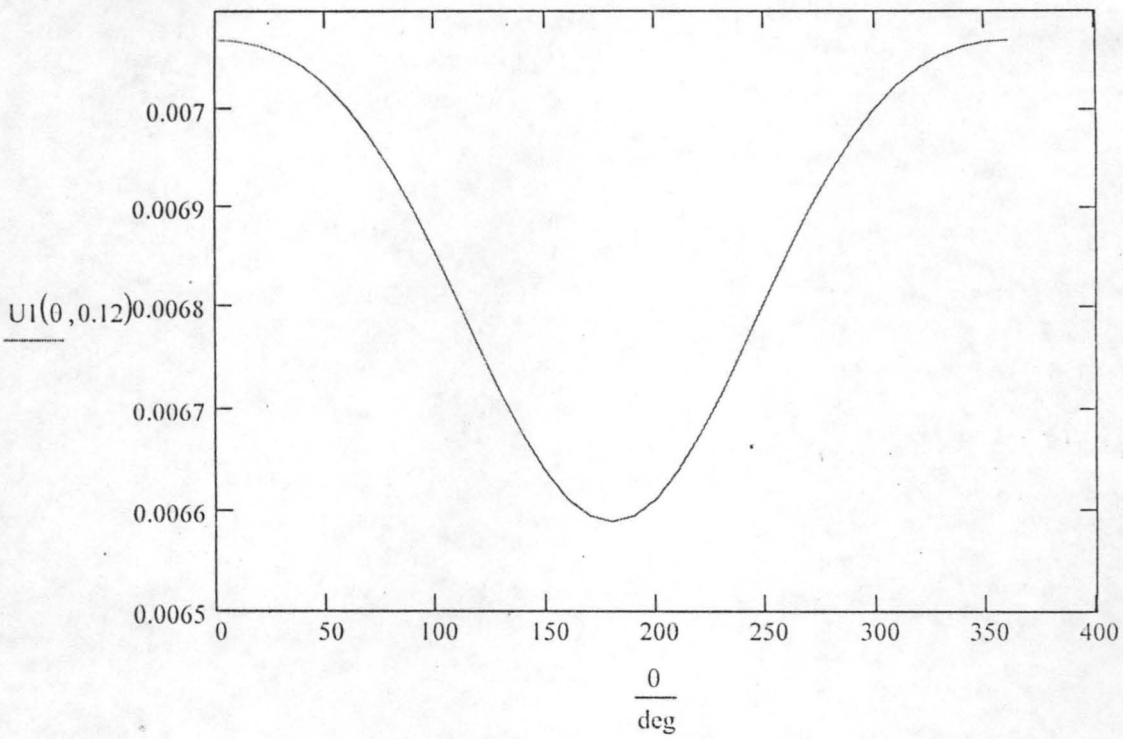


Graph 1: The flow pattern ( $mhu = 0.1$ )

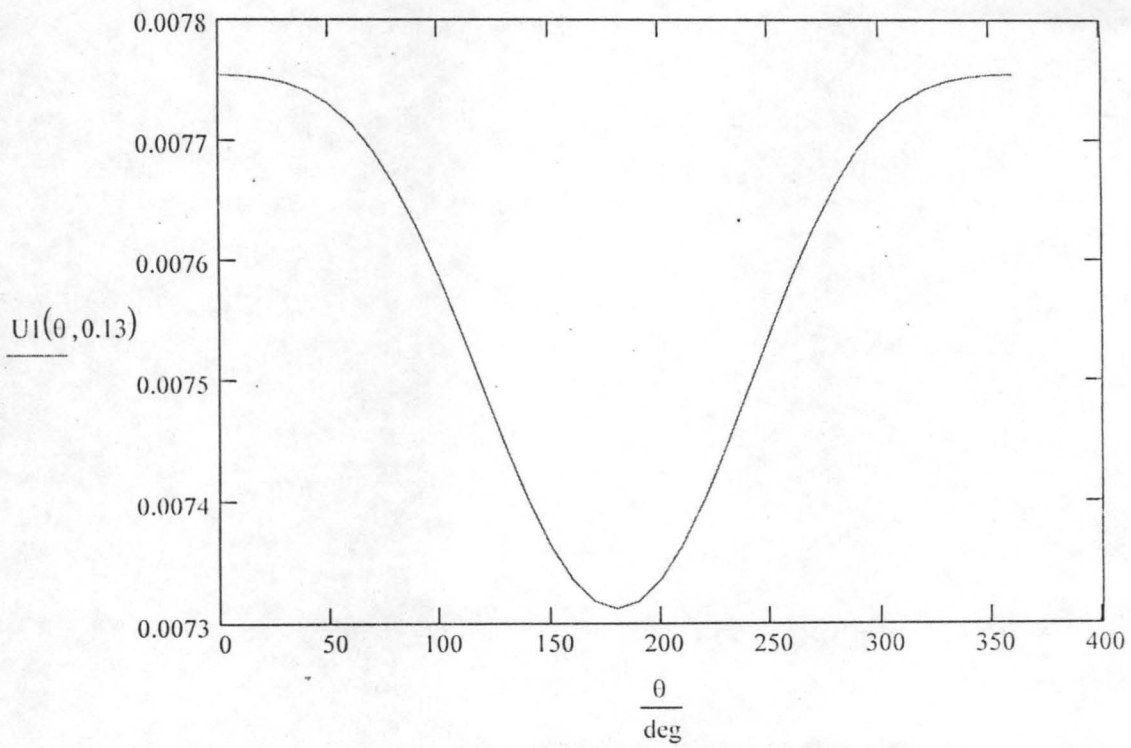


Graph 2: The flow pattern ( $mhu = 0.11$ )

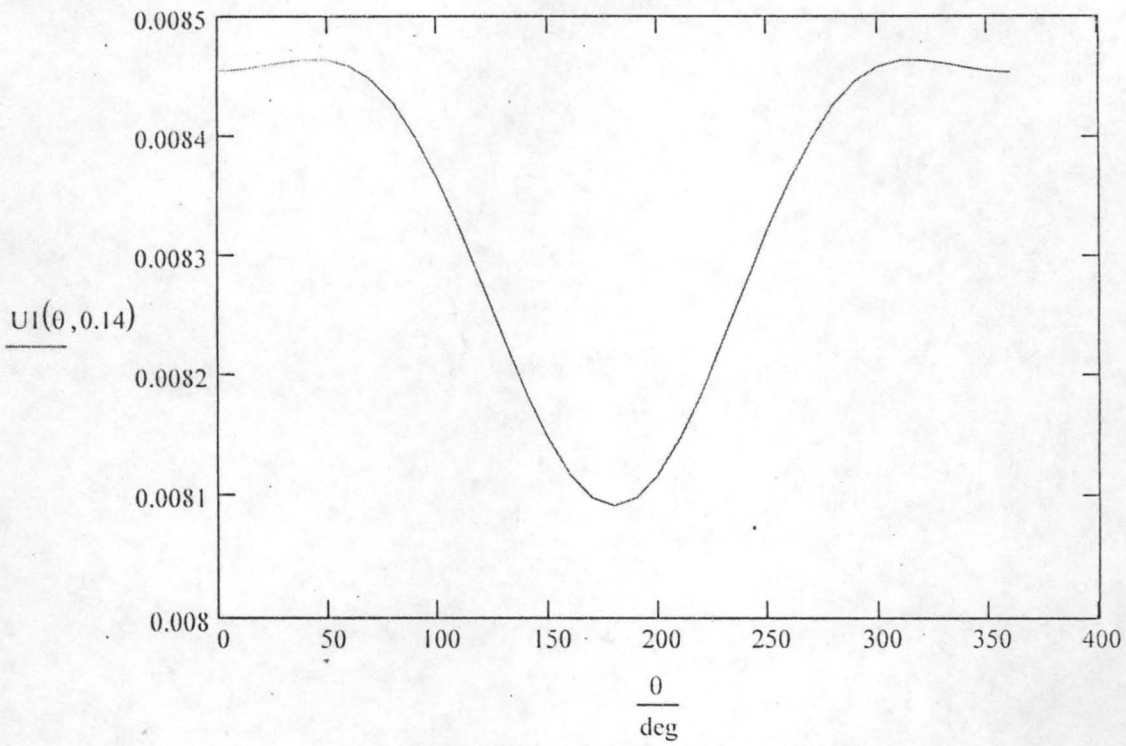




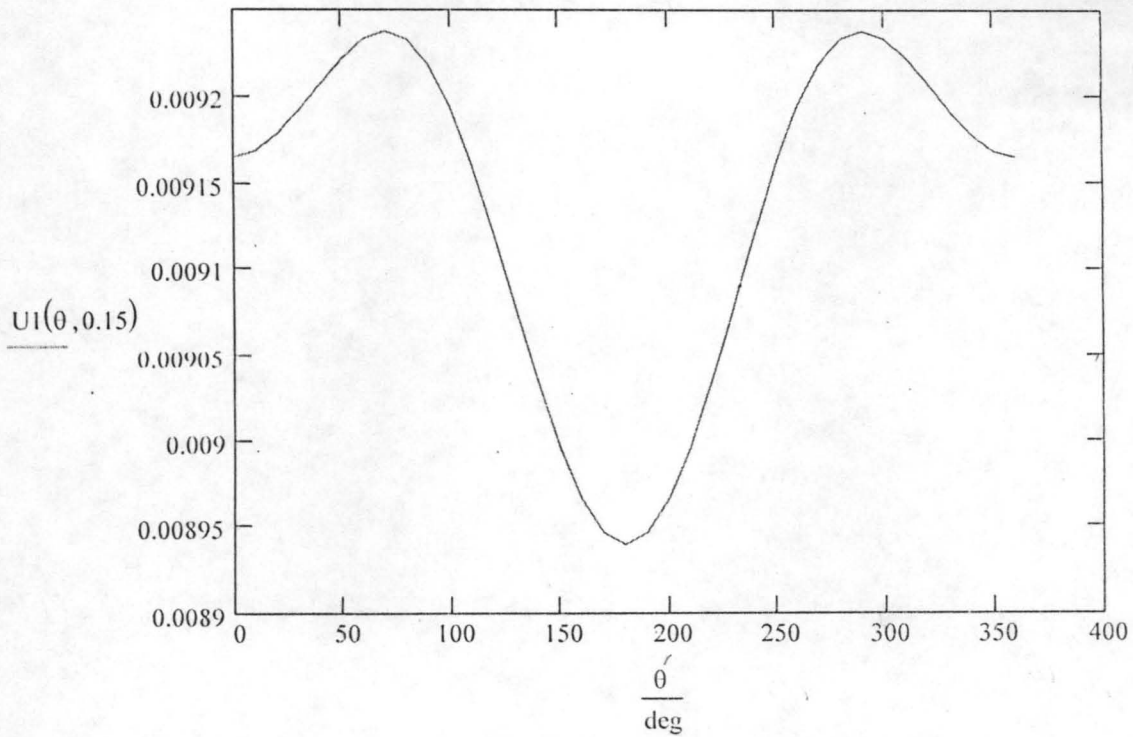
Graph 3: The flow pattern ( $mhu = 0.12$ )



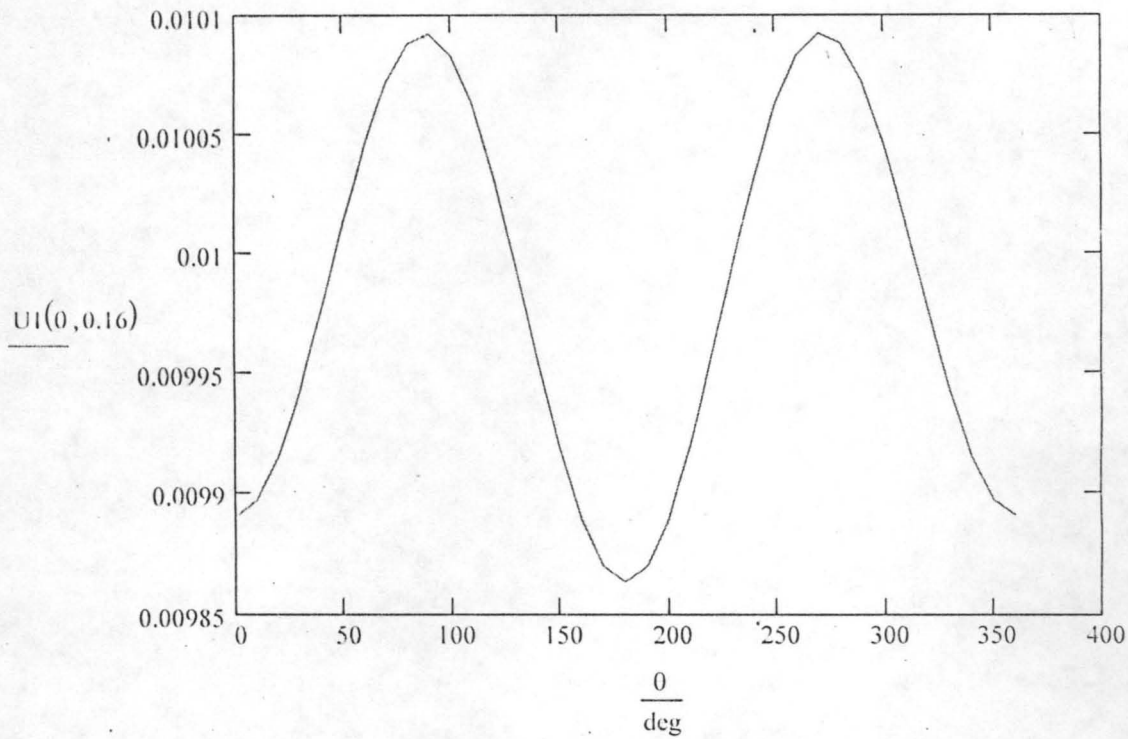
Graph 4: The flow pattern ( $mhu = 0.13$ )



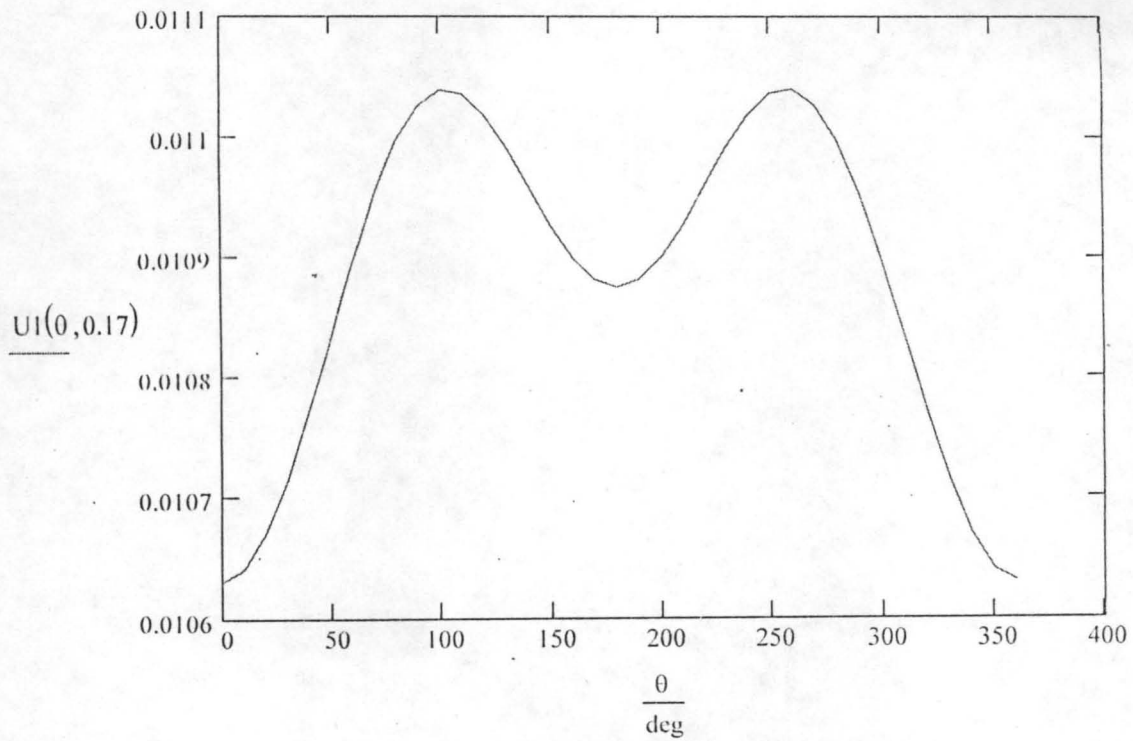
Graph 5: The flow pattern (mhu = 0.14)



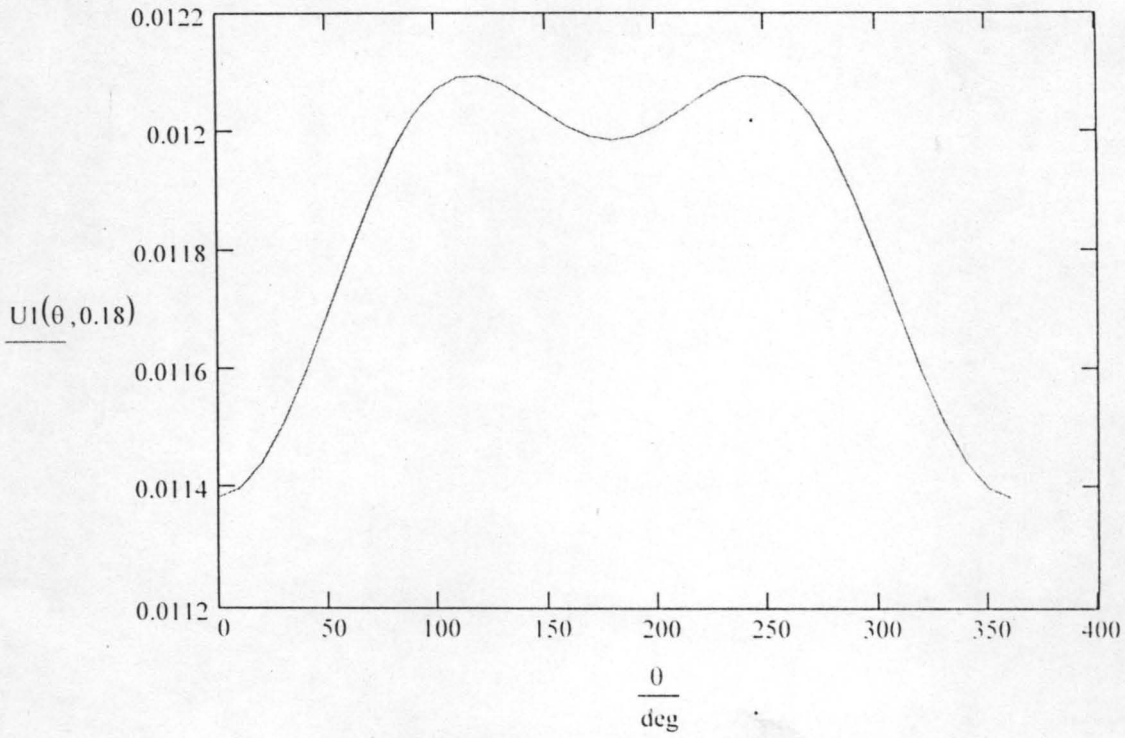
Graph 6: The flow pattern (mhu = 0.15)



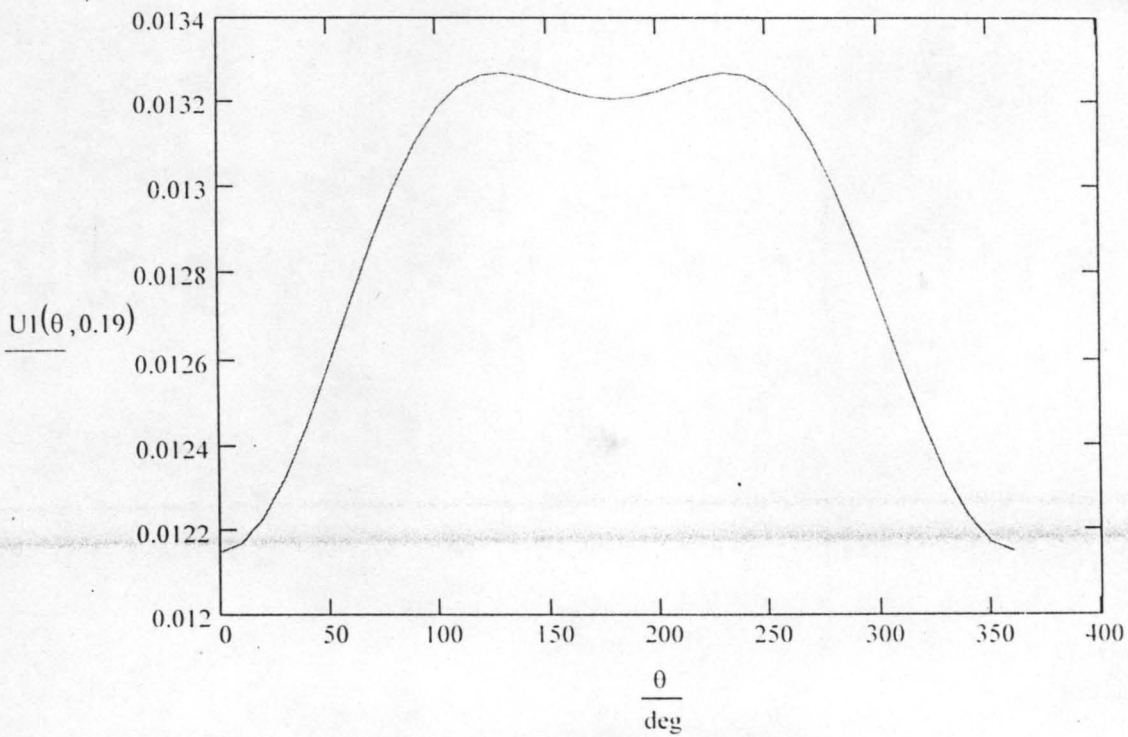
Graph 7: The flow pattern (mhu = 0.16)



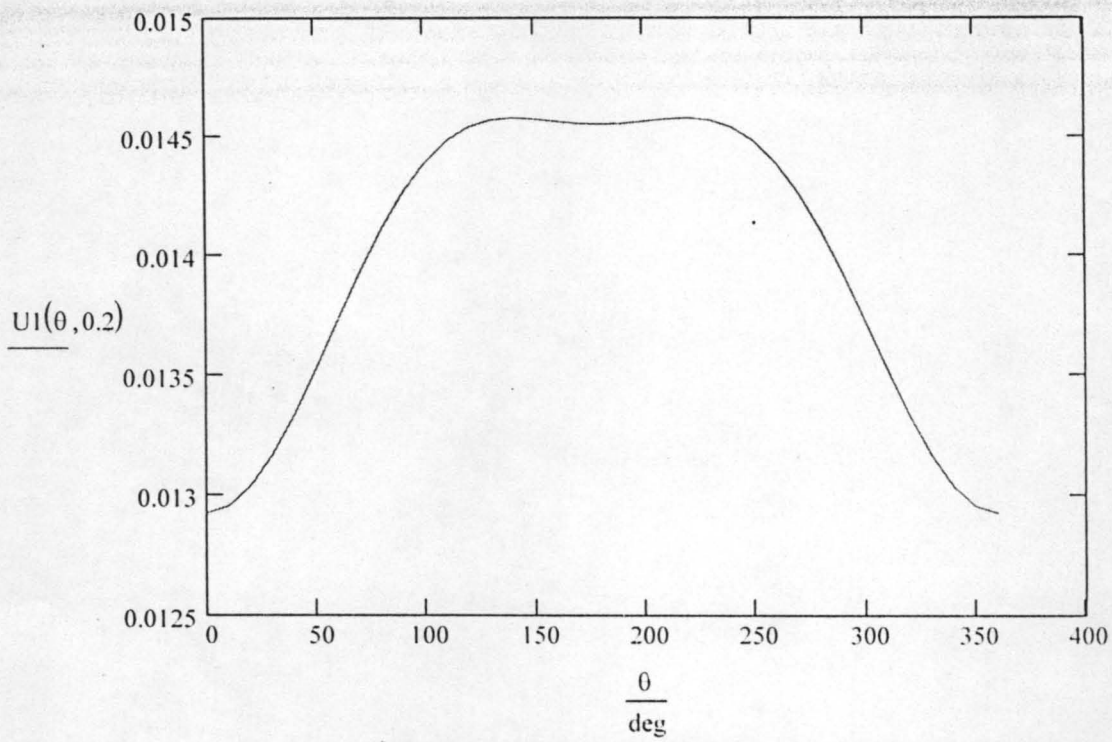
Graph 8: The flow pattern (mhu = 0.17)



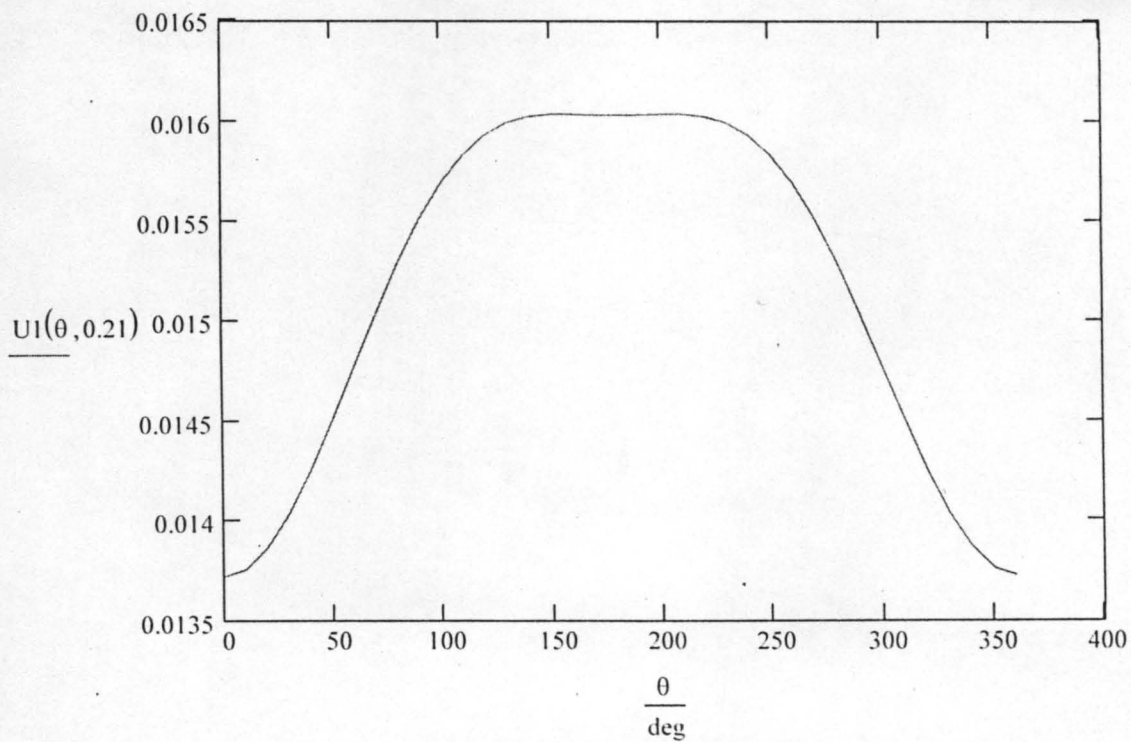
Graph 9: The flow pattern (mhu = 0.18)



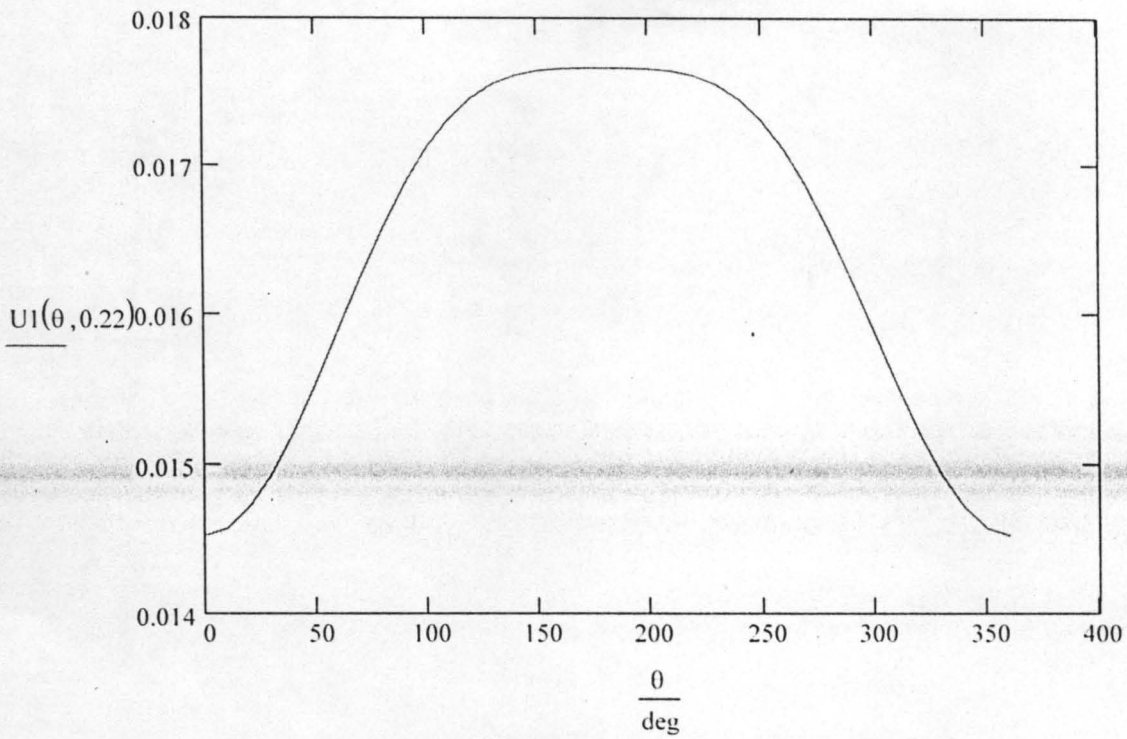
Graph 10: The flow pattern (mhu = 0.19)



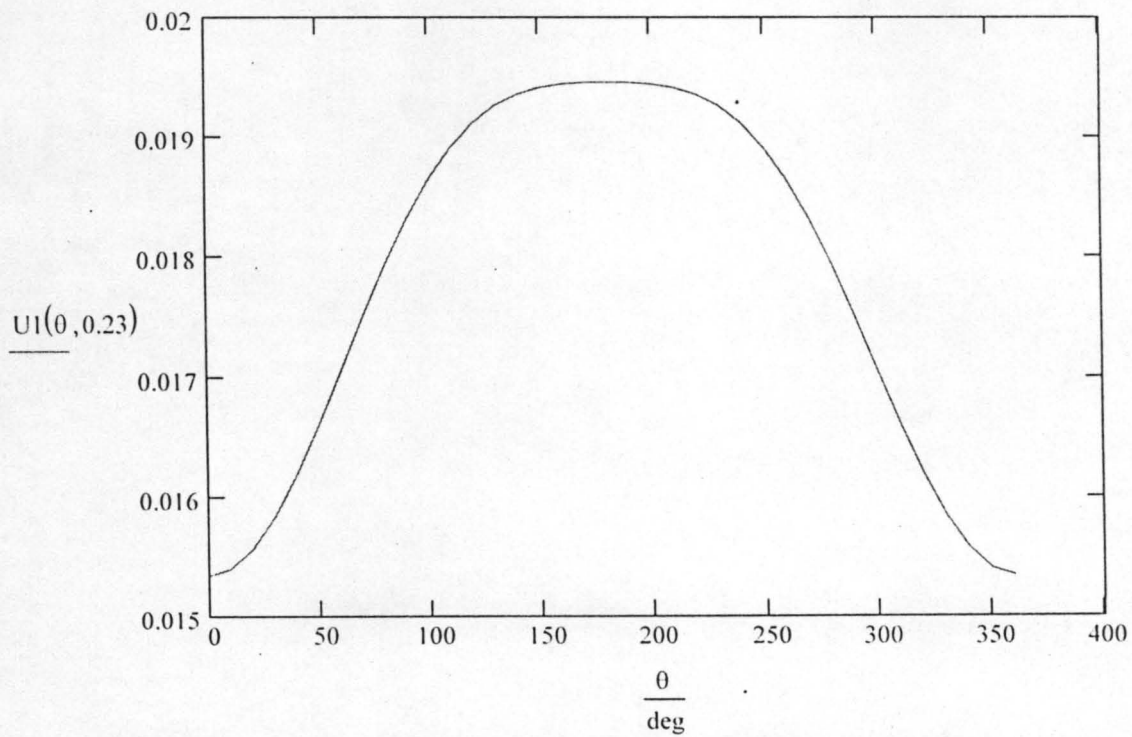
Graph 11: The flow pattern (mhu = 0.2)



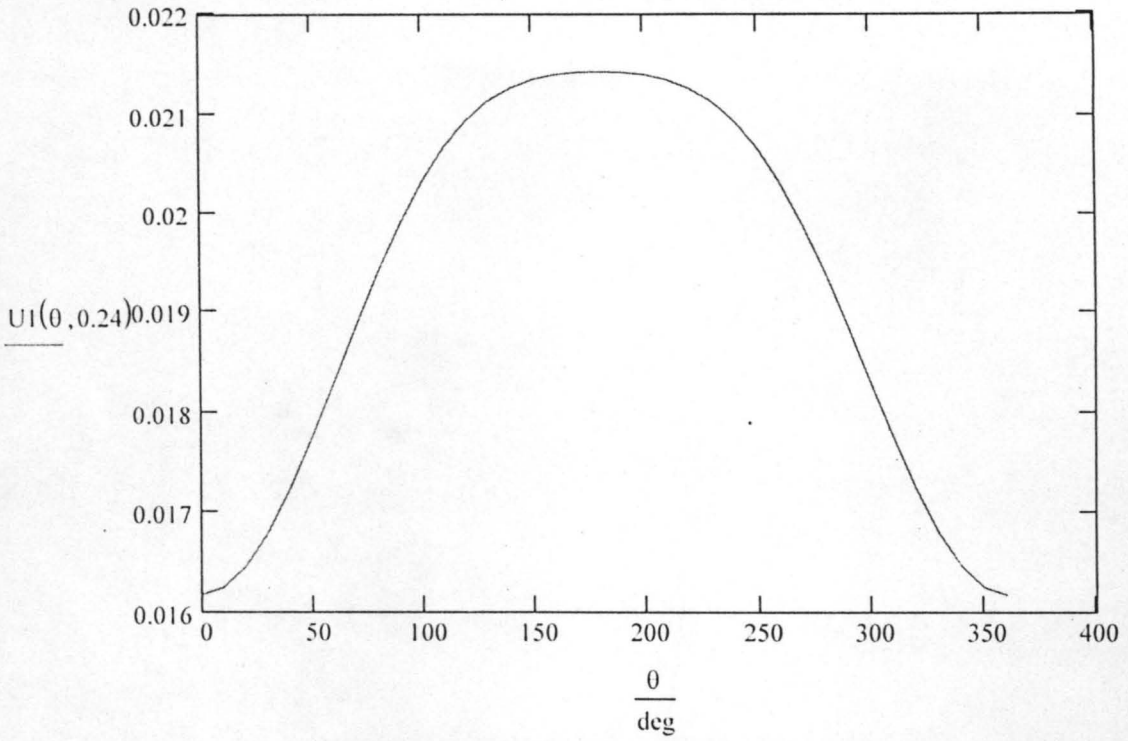
Graph 12: The flow pattern (mhu = 0.21)



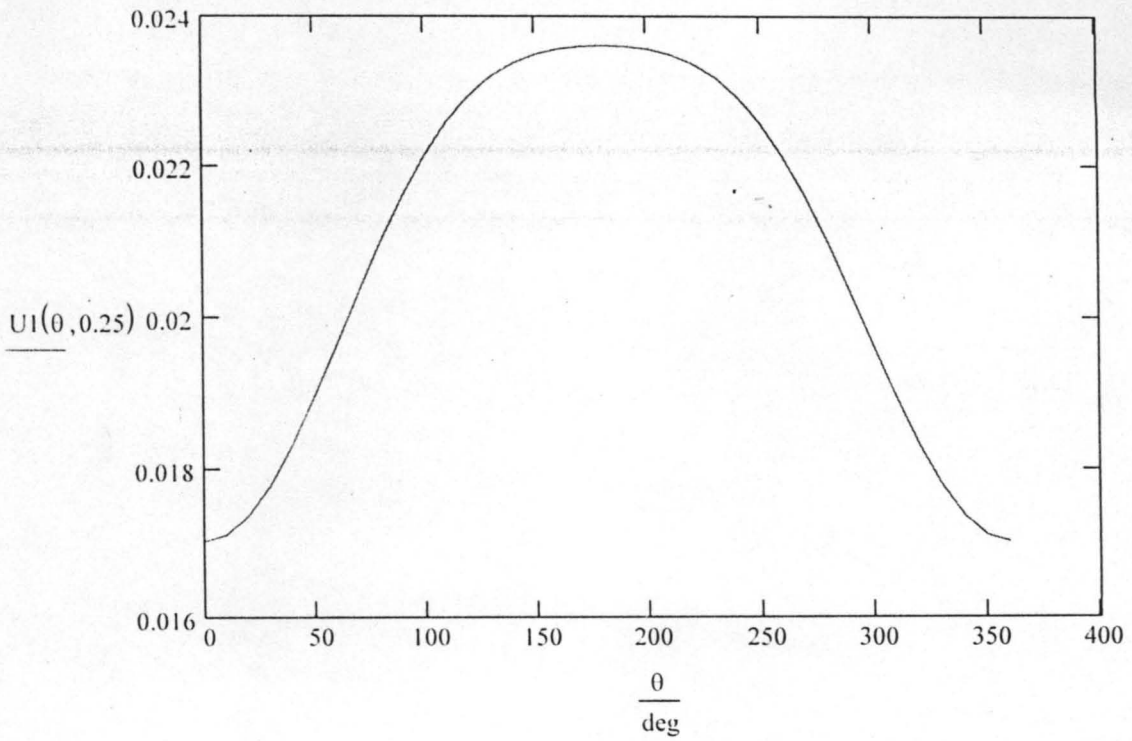
Graph 13: The flow pattern (mhu = 0.22)



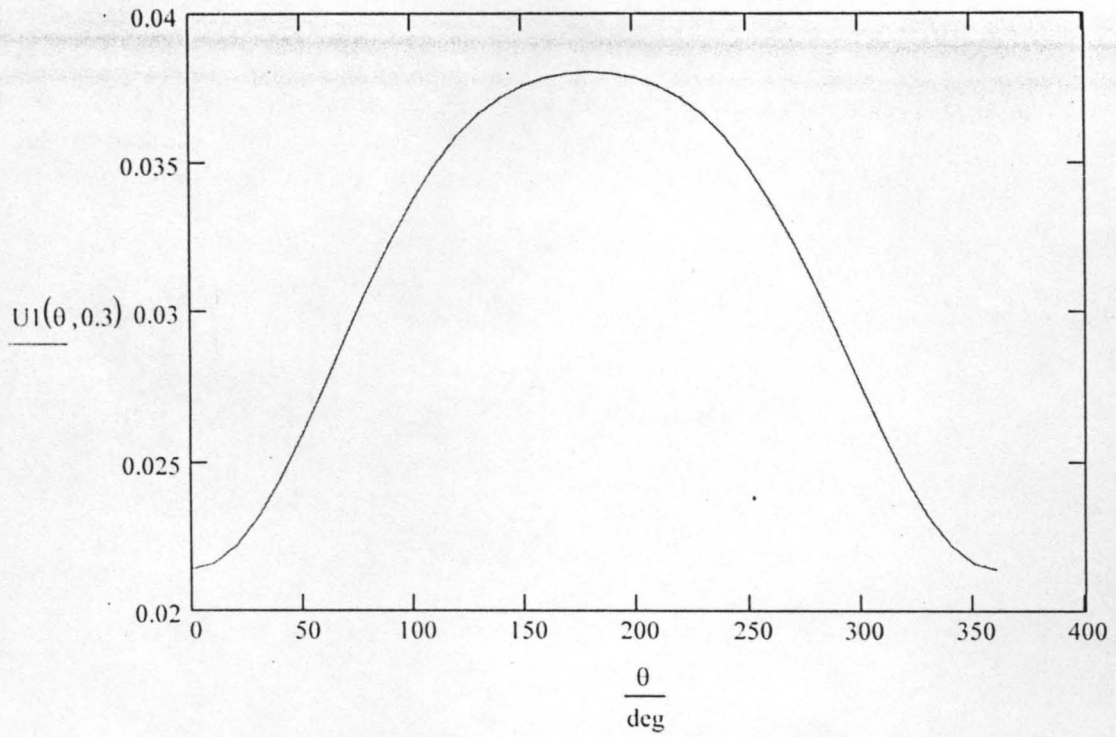
Graph 14: The flow pattern (mhu = 0.23)



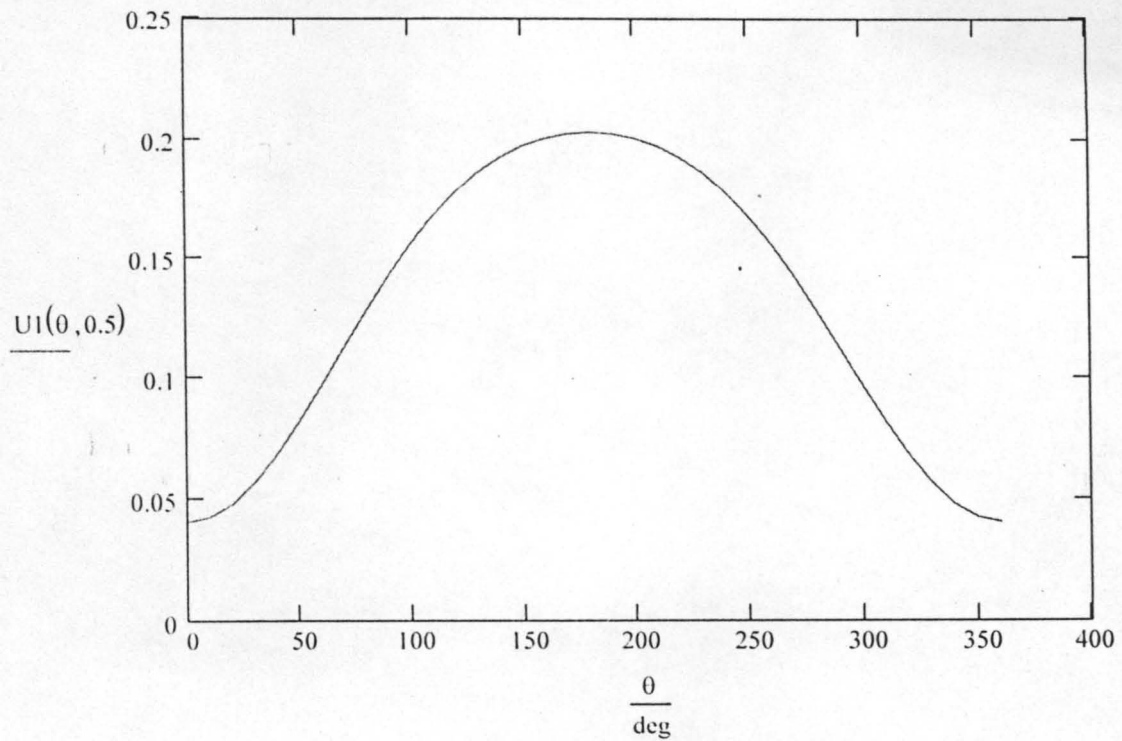
Graph 15: The flow pattern (mhu = 0.24)



Graph 16: The flow pattern (mhu = 0.25)

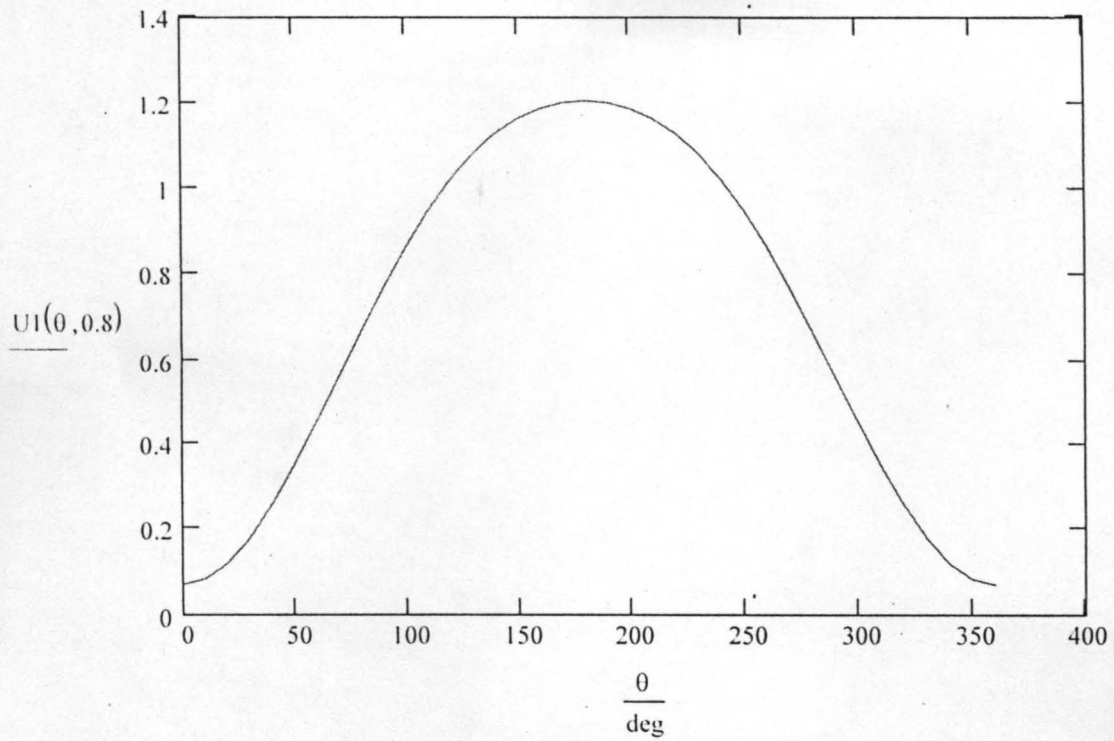


Graph 17: The flow pattern ( $mhu = 0.3$ )

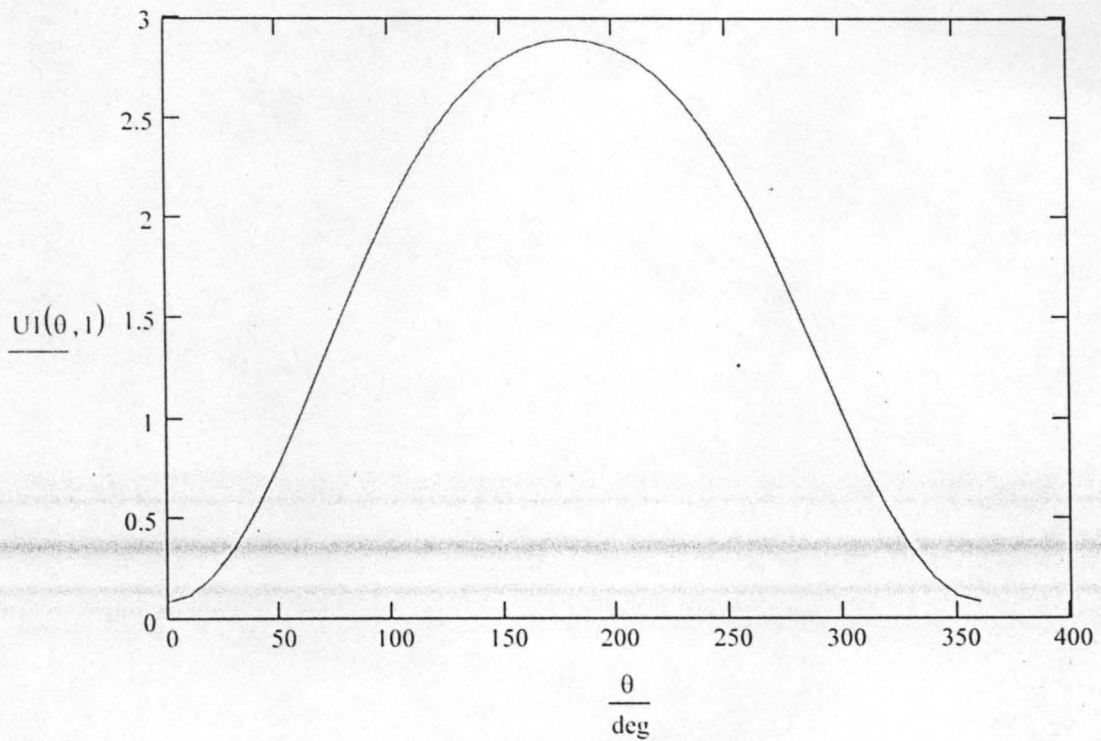


Graph 18: The flow pattern ( $mhu = 0.5$ )





Graph 19: The flow pattern ( $mhu = 0.8$ )



Graph 20: The flow pattern ( $mhu = 1$ )

## CHAPTER FIVE

### 5.1.0 Discussion and Summary

The flow past a sphere has been solved to the order  $\varepsilon^0$  equation and graphs of the flow were plotted for various values of  $a/r$ .

From the graphs, the flow pattern is discovered to be gaussian which is symmetrical about  $180^\circ$

The flow also increases steadily to a peak and then decreases, which shows that the flow is Lamina.

### 5.2.0 Conclusion and Recommendation

In this research, we have succeeded in analysing the flow past a sphere using the Legendre Polynomial functions for the order  $\varepsilon^0$  pertubation parameter and graphs were plotted showing the flow pattern.

Interested researcher may solve this problem for higher orders.

## REFERENCE/BIBLIOGRAPHY

1. K.F. Riley, M.P Hobson, S.J Bence:  
Mathematical Methods for Physics and Engineering Cambridge University Press 1998
2. Murray R. Spiegel:  
Theory and Problems of Advanced Mathematics for Engineers and scientists Shaums Outline series. McGraw Hill Metric edition 1974
3. Murray R. Spiegel:  
Theory and Problems of Advanced Calculus McGraw Hill Metric Edition. Shaums Outline series 1974
4. O.T Gideon:  
A regular Perturbation Analysis of the Non-Linear Contaminant Flow Equation M.Tech Thesis 2001
5. Rayput R.K:  
A Textbook of fluid mechanics S. Chand & Co Ltd. First edition 1998
6. Sir Hopace Lamb:  
Hydrodynamics Dover Publication New York 1932
7. William F. Hughes, John A. Brighton:  
Fluid Dynamics Second edition 1991 McGraw Hill.
8. Stokes G.G (1851)  
Camb. Phil. Trans. 9, 8
9. Proudman, I. and Pearson, J.R.A (1957)  
J. Fluid Mech. 2, 237
10. Chester, W. and Breach, D.R (1969)  
J. Fluid Mech. Vol. 37, Part 4 Pg 751